

## MILLENNIUM ENERGY CORPORATION

Claim 48: The applicant has added claim 48 to include a factor that is noted in the disclosure and raised by the examiner in the prior office action.

48. (new) A method of claim 34, wherein the working liquid is de-gassed prior to being put in a tension state.

The applicant respectfully submits the following response first to the comments of the examiner at the interview of September 25 2008 at which the entire draft Office action response was discussed, followed by a revised version of this Office action response.

In response to the examiner's request for clarification on how do we conclude that the observations from the experiment implies Thermo-nuclear Fusion.

Evidence for Thermonuclear Fusion in Bubble Nuclear Fusion Studies (Taleyarkhan et al.)

As indicated to the examiner in the interview of May 2007, in general, the fusion of deuterium(D)-deuterium(D) atoms is unequivocally established in the literature (Gross, 1984) to lead to one of two almost equally probable nuclear reactions. These are:

- The production of a 1.01 MeV tritium (T) nucleus and a 3.02 MeV proton.
- The production of a 0.82 MeV helium-3 ( $^3\text{He}$ ) nucleus and a 2.45 MeV neutron.

For the thermonuclear bubble fusion system, the tell-tale signatures of the event involve the measurement of 2.45 MeV neutrons which must be time-correlated with the time of bubble implosion (i.e., when the conditions are compressed and hot and light flashes are generated), the generation of gamma photons commensurate with neutron interactions with structural atoms, together with the generation of T nuclei at rates that are similar in rate to that for neutron production. In acoustic inertial confinement bubble nuclear fusion experiments (Taleyarkhan et al., 2002, 2004, 2006), the evidence for D-D fusion includes the following key findings of fact:

1. A statistically significant (4 to 5 Standard Deviations) production of tritium nuclei [Science (2002) – Fig. 3; Phys.Rev.E (2004)-Fig.11];
2. A statistically significant (4 to 25 Standard Deviations) number of 2.45 MeV neutrons [Science(2002)-Fig.4; Phys.Rev.E (2004)-Fig.8; Phys.Rev.Ltr (2006)-Fig.4];
3. An approximately equal number of D-D neutrons and T nuclei produced during any given experiment [Science(2002); Phys.Rev.E (2004)];
4. The generation of D-D neutrons time correlated with sonoluminescence (SL) flashes during deuterated bubble cluster implosions [Science(2002)-Fig.5; Phys.Rev.E (2004)-Fig.7];
5. The subsequent (to neutron and SL) emission of statistically significant quantities of gamma rays due to D-D neutron capture in hydrogen and other atoms of surrounding structures and in the detector; the ratio of gammas to neutrons being about 0.05 to about 0.15, and the energy of the gamma rays being ~ 2 MeV as to be anticipated [Phys.Rev.E (2004)-Figs.9,10];
6. The attainment of null results (i.e., no neutron, gamma or tritium emissions) for corresponding control experiments under identical conditions but with the *only variation being change of the D atoms in test liquids to H atoms* [Science (2002), Phys.Rev.E (2004), Phys.Rev.Ltr (2006);

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7. The consistency of the experimentally-observed results of neutrons and tritium with theory which, after considering all key physical phenomena associated with growth and implosion dynamics, reveal and predict conditions required for thermonuclear fusion (i.e., 1000+ GPa compression pressures and  $\sim 10^8$  K plasma states) to occur only under the conditions of successful experiments. The same theoretical framework predicts non-attainment of such conditions for non-ideal thermal hydraulic conditions, as well as for low-accommodation coefficient fluids such as heavy water for similar experiment conditions – an aspect which is consistent with experimental findings, [Phys. Fluids (2005)-Fig.13, Science (2002)-Fig. 6];
8. The verification and confirmation of the neutron and tritium emission data by unaffiliated groups [Nucl.Engr.Design (2005); NURETH-11 (2005); Trans.Amer.Soc.(2006); Int.Fus.EnergyMtg.(2006); Bugg Report (2006); Public Demonstration Testimonials (2006)];
9. The consistency of neutron emission spectra from 5 separate reports with validated nuclear infrastructure methodologies utilizing state-of-art Monte-Carlo 3-D nuclear particle transport simulation tools (MCNP5 and SCINFUL) developed under U.S. DoE sponsorship at Los Alamos National Laboratory and Oak Ridge National Laboratory – as evidenced in Nucl. Engr. Des.(2008) – Figs. 6, 7, 9, 11]; and,
10. Testimonials of successful demonstrations on two separate occasions to collection of industry, government and academic bodies [IDI testimonials, 2006]].

With regard to the issues raised by the examiner in the Office Action:

1. The examiner claims that the applicant has elected in his response of 7/12/05 Group II Process, Species G(D-T) reaction and Species 1 (acoustical wave source).

- 1.1. The applicant respectfully submits that the election was with traverse and with regard to the election of species G has noted for example in that response that claims 23 and 27 are readable on D-T reactions.

- 1.2. The applicant further submits that a D-D reaction envelopes the conditions for a D-T reaction and provides for the record art that establishes factual experimental underpinnings. (reference: "Gross., R. A., 1984 "Fusion Energy" John Wiley & Sons.) Therefore, the applicant submits that the D-T reactions will occur if conditions for D-D reactions are provided as indicated in the Response of 2008-5-21 as experimental evidence of this reaction phenomenon.

Therefore the applicant respectfully requests the examiner to: Firstly, allow the revised claim 47 – now a method claim in the elected Invention I, and now with support for the factual experimental underpinnings for the D-T reaction; and Secondly, allow the generic claim, considering that the reaction conditions of the invention provide the requirements for either or both of the D-T and D-D reactions.

2. The examiner claims that the following submissions lacked probity for enablement & utility because they were established after the filing date :

- a) Findings (Fig. 7c) in the premier journal Physical Review E, Vol. 69, 036109-1 to 11, by Taleyarkhan et al., 2004 that demonstrates experimentally that D-D fusion neutrons of 2.45 MeV in energy as required for thermonuclear fusion are emitted in a time –correlated manner with the emission of sonoluminescence (SL) light flashes demonstrating that the fusion reactions are occurring under hot, compressed conditions for the method and apparatus of this present invention application.

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- b) The theoretical foundation for supercompression-induced thermonuclear fusion for the experimental conditions of the method used for the current application. This theoretical foundation takes into account all relevant physics and chemistry of the condition. It has passed worldwide peer reviews and validated by experts as being on sound theoretical foundations and published in the prestigious journal Physics of Fluids (Nigmatulin et al., 2005). This theoretical foundation when applied specifically to the method of the present invention confirms thermonuclear conditions (see Fig. 13 of the paper by Nigmatulin et al., 2005 – Physics of Fluids, Vol.17, 107106, 2005) with temperatures and pressures reaching in the range of  $10^8$ K, and 1000+ Mbar, respectively – convincingly thermonuclear fusion conditions.
- c) Three independent replications of published sonofusion results (Nuclear Engineering and Design journal paper, Vol. 235, pp.1317-1324 by Xu et al., 2005; Archives of Trans. American Nuclear Society, Vol. 95, pp. 736-737, by Forringer et al., 2006; Le Tourneau University, Texas, Press Release, 2006; and the Bugg, W confirmation report dated June 9, 2006 to Purdue University of 2006) of the present invention. Proof of reproducibility and repeatability and confirmation of successful fusion signals attainment following the apparatus and operations of this 10/692,755 Application from published documents were reproduced for the examiner.

The applicant respectfully submits first that the probity of the invention is established in the IDS filed October 27, 2003 of results of the present invention with experimental evidence preceding the filing: "Evidence for Nuclear Emissions during Acoustic Cavitation". R.P.Taleyarkhan et al. Science 8 March 2002, Volume 295 pp1868-1873.

Moreover, further support is provided in the paper on theoretical foundations "The Analysis of Bubble Implosion Dynamics" Supplement #2 (Reference 25 in the above IDS) and as published in Science: [www.sciencemag.org/cgi/content/full/295/5561/1868/DC1](http://www.sciencemag.org/cgi/content/full/295/5561/1868/DC1).

The additional materials noted by the examiner were discussed with the examiner at the interview on May 21, 2007 to provide additional irrefutable evidence of the validity of the results of the present invention.

Item 2.a) is an experimental study reported in a reputable peer reviewed Journal that further supports enablement of the method and apparatus of the present invention for producing 2.45MeV neutrons required for nuclear fusion, in a correlated manner to the emission of sonoluminescence light flashes. The approach uses the identical apparatus as noted in the invention with the exception of more sophisticated neutron detection approaches to get an even better statistically significant result. Nothing in the observable ambient universe that could affect this experiment is known to have changed between the date of filing and this duplicate experiment, and therefore the results provide additional clear probity for the invention.

Item 2.b) is a theoretical foundation for supercompression-induced thermonuclear fusion for the experimental method and apparatus of the present invention. Published in a peer reviewed Journal. This theoretical result that further supports the results of the invention by design addresses the methods and apparatus of the present invention. Therefore it provides additional clear probity for the present invention.

Item 2.c) consists of three successful replications of the invention as filed. These replications used the same methods and design of apparatus of the present invention. The applicant in addition submits herewith affidavits under 37CFR 132 in support thereof.

Nothing in the observable ambient universe is known to have changed with regard to the present invention between the filing date of the invention and the dates of these experimental results.

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Therefore these three successful replication results provide three more additional references for clear probity for the present invention.

The applicant respectfully submits that the probity of enablement has been established with the filed IDS and in addition the evidence as above reported in reputable peer reviewed journals and the integrity of three separate replications with Affidavits provided under 37CFR132.

Furthermore, the applicant submits as attached, herewith yet another additional confirmation for the validity of the thermo-nuclear fusion results " Modeling Analysis and prediction of neutron emission spectra from acoustic cavitation bubble fusion experiments" Nuclear Engineering and Design 238 (20082779-2791) along with these affidavits.

3. The examiner rejects claim 34 as he states:

Claim 34 recites the limitation, "placing at least a portion of said liquid into a tension state, a maximum tension in said tension state being below the cavitation threshold of said liquid." There is neither an adequate description nor enabling disclosure as to how and in what manner one can determine: a) that a portion of the liquid is in the so-called tension state; b) the maximum tension in a portion of the liquid in a tension state; and c) that the maximum tension is below the cavitation threshold of the liquid


The applicant respectfully submits that:

- 3.1. There exists a tension state for liquids achievable with tensile forces on the target volume of the liquids. For example even in nature mechanical motion of vascular passages of plants lead to liquid in tension. (Reference: Scholander., P. F., "Sap pressure in vascular plants" Science Volume 18, pp 339-345 16 April 1965.)
- 3.2. Therefore a portion of the liquid may be reduced to the tensioned state by applying a tensile force to the container walls that is by design in contact with the liquid. Such a force may be effected by a mechanical device as in the present invention that may be centrifugal force or oscillations of the wall by an electro-mechanical device. Such force enabling by these two phenomena are well established in the background art. The magnitude of the noted force can be increased by design to ensure that the liquid is at a desired level of the tension state.
- 3.3. The specification teaches the regions of the liquid that are in tension as a result of the apparatus design. For example originally filed Specification page 47 line 15-18 and Page 39 lines 19-21. (para [0135] and para [0167] as published).
- 3.4. There exists a cavitation threshold for such tensioned liquids by audible and visible inspection at adequate drive power of the mechanical force in the presence of nucleating particles.
- 3.5. The method or apparatus of the invention can achieve and exceed such a cavitation threshold by design as in 3.2 above, as a result of 3.3 above.

Therefore the applicant respectfully submits that the enablement requirement is met with the background art.

4. The examiner further states:

Claim 34 further recites, "imploding said bubbles substantially filled with vapor." There is neither an adequate description nor enabling disclosure as to how and in what manner one: a) can determine when a bubble has been substantially filled with vapor; b) identify which of the bubbles that are allegedly substantially filled with vapor; and c) how many of these bubbles to implode to induce a nuclear fusion reaction.

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The applicant respectfully submits that:

- 4.1. The background Art is replete with exposition that any fluid will exert a vapor pressure in an adjoining space and therefore such bubbles are substantially filled with vapor of the parent liquid as disclosed. As there are no other liquids in contact with the bubble surface therefore there is no other vapor pressure exerted. Moreover, considering that there is no attempt to intentionally dissolve gases in the parent liquid the resulting partial pressures if any such gases are small, however as the parent liquid at some point may have had a surface open to a gas such as the constituent gases of the atmosphere, there is likely to be some -- even minute quantities -- of preexisting dissolved gas in the parent fluid. Therefore the applicant submits that all such bubbles are substantially filled with vapor of the parent liquid.
- 4.2. One or more such imploding bubbles create nuclear fusion as substantiated in the experimental observation results of the disclosure. The nature of bubbles that create nuclear fusion are defined in the Specification Page 18 lines 20-21 page 19 lines 1-4.

Therefore the applicant respectfully submits that the disclosure in conjunction with the background art is enabling.

5. On claim 42, the examiner states:

Claim 42 recites, "synchronizing neutron impact with a location in said liquid having a predetermined liquid tension level." There is neither an adequate description nor enabling disclosure as to how and in what manner one: a) can determine the occurrence of an impact of the neutron with the pre-tensioned liquid; b) synchronizes the neutron impact with a location in said liquid; c) determines which specific location to direct the impact of the neutron.

The applicant respectfully submits that the specification discloses the production of tensioning of the liquid in synchronization with the nucleating particles. Fig 3, Page 21 lines 8-15, Page 25 lines 3-20, of the original Specification.

The nucleating particles are directed in the direction of the chamber and therefore those that reach the liquid during the above tension state are capable of nucleating 10-100nm size bubbles. It is established in the background art that nucleating particles can nucleate bubbles of this size in meta-stable liquids. Reference: Glaser, D. A., Phys. Rev., Vol.87, 665, 1952.

Therefore the applicant respectfully submits that the disclosure in conjunction with the background art is enabling.

6. The examiner rejects claims 34-46 as he notes that on claim 34:

In amended claim 34, applicant has deleted the step, "degassing said liquid to reduce a dissolved gas content therein, wherein said dissolved gas is removed using an applied vacuum." Note the following passages in the specification that demonstrate criticality of the degassing step in the exercise of the claimed invention:

*"To minimize the effect of gas cushioning during implosive collapse, the working liquid can be degassed, a priori. Alternatively or in combination, a sufficient vacuum state above the working liquid accompanied by induction of gaseous cavitation induced by nuclear particles such as neutrons or via use of lasers or acoustic horns can be used to reduce the dissolved gas content in the working liquid to limit unwanted gas cushioning."*  
See page 17, last paragraph.

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*Following degassing of the working liquid, the liquid is tensioned and nucleation of vapor cavities followed by implosion of the same can be initiated. Tensioning the liquid can be provided by a variety of methods, including an acoustical wave source, an electrostrictive (piezoelectric) source, a magnetostrictive source, a centrifugal source, a focused (pulsed) acoustic energy or a venturi based system. Preferably, when an acoustical wave source is used, the acoustical wave source includes an acoustical focusing device, such as a parabolic-type reflector or a resonant cavity to intensify the acoustic pressure. See page 17, last paragraph.*

The applicant respectfully submits that the degassing step is an *optional* step to enhance the operation of the method or apparatus even as stated in the above by the examiner:

*"To minimize the effect of gas cushioning during implosive collapse, the working liquid can be degassed, a priori." (emphasis provided)*

The applicant therefore respectfully submits that the claim as amended is consistent with the original disclosure and requests the allowance of claims 34-46.

7. The examiner notes that Claim 44 recites the limitation "said fundamental particles" in lines 1 and 2. There is insufficient antecedent basis for this limitation in the claim.

The applicant agrees with the examiner and has amended claim 34 to be consistent.

8. The examiner notes in claim 46 that:

The term "high accommodation coefficient liquid" in claim 46 is a relative term which renders the claim indefinite. The term "high" is not defined by the claim, the specification does not provide a standard for ascertaining the requisite degree, and one of ordinary skill in the art would not be reasonably apprised of the scope of the invention.

The applicant respectfully submits that the specification makes clear what high and low mean. High accommodation coefficient is stated to be ~1.0 (the maximum) the value associated with organic liquids such as acetone, benzene, tetrachloroethylene whereas, low is stated to be closer to 0 citing the value for water at ~ 0.07 which is not recommended for enhanced fusion induction capability. See for example Specification as filed for experimental results page 16 lines 8-20 and validating theoretical foundations Page 70 lines 14-20, Page 71 lines 1-8.

Moreover, the background art has definitions for high accommodation liquids accessible to those with ordinary skill in the art for example. Reference 25 in the IDS of 2003.

35USC 102 Rejections

9. The examiner states in support of rejection of claims 34-40, 42, 44 and 45:

Claims 34-40, 42, 44 and 45 are rejected under 35 U.S.C. 102(b) as being anticipated by either one of Margulis (RU 2096934) or Lipson et al., "Initiation of fusion reactions in

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media containing deuterium by cavitation," Soviet Physics: Technical Physics 37 (1992) Margulis.

In particularly with regard to claims 34, 35, 37-40, 42, 44 and 45 the examiner states:

- As to claims 34, 35, 37-40, 44 and 45, Margulis discloses a method for generation of high-temperature plasma and generating thermonuclear reactions by providing a liquid enriched with a mixture of deuterium and tritium, creating tension microbubbles containing such mixture by ultrasonic vibrations and thereby generating thermonuclear reactions.
- Applicant has not defined which portion of the working liquid is placed in a maximum tension below the cavitation threshold. Absent such definition, the examiner interprets the term broadly and reads it on any and all portions of the working liquid.
- Accordingly, one can always find a portion of the liquid in Margulis that has such maximum tension below the cavitation threshold.
- As to the claimed "nucleating agents", the thermonuclear reactions in Margulis inherently produce at least neutrons and photons, and these are inherently directed to the tensioned liquid because said particles and said liquid are in the same contained volume of the apparatus.
- As to the bubbles being substantially filled with vapor, applicant has not defined the term substantially filled, and the examiner interprets this term broadly to read on any degree of filling that occupies most of the internal volume of a bubble.
- One can always find a plurality of bubbles in Margulis that is mostly filled with vapor because of the heat produced from the thermonuclear reaction .
- As to the growing of the bubbles and the temperature generated from the system, note page 6, last 2 lines in the English language translation of Margulis.

The applicant respectfully submits that there are fundamental differences between Margulis and the present invention as claimed in Claim 34 and its dependant claims:

- 9.1. Margulis requires a liquid under *positive pressure* for their reactions – it is a compressed liquid. Margulis *requires gas insertion* into the liquid for their process. Nowhere in Margulis is there reference to tensioned liquids. (Tensioned liquids have an absolute pressure of less than zero). In fact tensioned fluids cannot support the required seeding of D and/or T enriched and saturated gas bubbles together an inert gas, required for operation of Margulis. In contrast, the present invention requires a tension state as stated in claim 34, but no gas bubbles as required by Margulis.
- 9.2. Margulis is enabled by the introduction of gas bubbles containing D and/or T atoms and an an inert gas to saturate the parent fluid. The present invention *introduces the target D and/or T atoms by vaporizing the parent liquid*. There is no enablement requirement with gas bubbles in the present

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invention. Claim 34 and its dependants clearly state the working liquid to be enriched with D and/or T atoms and does not depend on any inserted gases.

- 9.3. Margulis with the gas saturated fluid cannot sustain a tension state. The background art is replete with examples of foaming of liquids saturated with gas as an inherent limitation for tensioning. For example consider the analogy of a gas saturated soda bottle that is opened to atmospheric pressure. Therefore the requirement of a tensioned liquid is not possible in Margulis. Therefore, tension micro-bubbles cannot be formed in Margulis. Therefore, for Margulis, even if nucleating particles are present, considering that a tension state is not attained, the conditions for these particles to initiate cavitation bubbles in a tension state in the liquid will clearly not be met.
- 9.4. If thermo-nuclear fusion occurs in Margulis, then neutrons produced will be when the gas bubbles are compressed therefore the liquid will be under positive pressure and not tension. Therefore there is no parallel between the present invention and Margulis on the nucleating agents.
- 9.5. If thermonuclear fusion occurs in Margulis, then it is true that there will be soon thereafter, rise in the temperature in the predominantly gas bubble. However, there is *no possibility* of the bubbles being substantially filled with vapor *before* such a thermonuclear fusion reaction occurs – if such a reaction were to occur in Margulis. The bubbles in Margulis are by design filled with a D and/or T enriched gas unrelated to the liquid.

The applicant submits therefore that claim 34, 35, 37-40, 45 are not anticipated by Margulis and should be allowed.

The examiner notes on Claim 36:

As to claim 36, Margulis teaches the use of heat exchangers for cooling (see page 11 of the English language translation).

The applicant respectfully submits that there are fundamental differences between Margulis and the present invention as claimed in Claim 36:

- 9.6. In addition to the factors noted above that distinguish Margulis from the present invention, Margulis uses two heat exchangers. The first to *heat* the liquid and the second to convect away heat created from a possible thermonuclear reaction by neutrons penetrating a blanket. In contrast the present invention *cools* the liquid to below an ambient temperature as noted in claim 36.

The applicant submits therefore that claim 36 is not anticipated by Margulis on this factor as well. The applicant respectfully submits that this claim should therefore be allowed.

The examiner further notes on Claim 42:

As to claim 42, applicant's claim language, "neutron source" reads on the fusion reactions in Margulis that inherently produce neutrons.

The applicant respectfully submits that there are fundamental differences between Margulis and the present invention as claimed in Claim 42:

- 9.7. The applicant respectfully submits that if neutrons are produced with a possible thermonuclear reaction, such neutrons are available only under positive pressure and

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therefore cannot nucleate bubbles. In contrast with the present invention where the neutrons are utilized during a tension phase of the process. Therefore Margulis does not read on the present invention on this factor as well. The applicant respectfully submits that this claim should therefore be allowed.

(Lipson et al)

10. The examiner states in support of rejection of claims 34-40,42,44 and 45:

- As to claims 34,35,37-40,44, and 45, Lipson et al., disclose a method for creating fusion reactions in media containing deuterium by cavitation. (As to the interpretation of the undefined terms in applicant's claim, the discussion above relating to Margulis applies also to Lipson et al.).
- As to the nucleating agents, Lipson et al. discloses the generation of neutrons (see page 1191, col. 2, last paragraph)
- As to tensioning of the liquid below the cavitation threshold, growth of the bubbles and their collapse, see page 1190, bottom of col. 1 and top of col. 2.
- As to claim 36, Lipson et al. disclose a cooled vessel (see page 1190, col. 2, "Experimental Apparatus and Procedure").
- As to claim 42, applicant's claim language, "neutron source" reads on the fusion reactions in Lipson et al. that inherently produce neutrons.

The applicant respectfully submits that there are fundamental differences between Lipson and the present invention as claimed in Claims 34, 35, 37-40,44 and 45:

- 10.1. Lipson is enabled by a vibrating metal projection within a liquid enriched with D, wherein the metal can absorb the D. the present invention does not require such metal protrusions and the claims noted by the examiner have no reference to such metal protrusions.
- 10.2. Lipson states (pp1191 last para): "It follows that assumptions 1 and 2 regarding the possible generation of neutrons during the collapse of cavitation bubbles, either directly in the D<sub>2</sub>O or on the metal surface of the vibrator, *find no support from these results*". (Emphasis provided) The disclosure by Lipson therefore does not support the examiner's claim.
- 10.3. Lipson speculates that there may be conditions for neutron emission during the growth and collapse of cavitation bubbles in D<sub>2</sub>O *enabled by* the metal surface of the protrusion or vibrator. The present invention does not require a metal vibrator.
- 10.4. In Lipson the liquid with cavitation bubbles are at positive pressures and not in a tension state of the liquid as in the present invention.
- 10.5. Lipson uses a temperature of 30 C  $\pm$  10 C and cools his apparatus to this range. The present invention may be cooled below ambient as claimed. Any scientific apparatus may be

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cooled to a required range of optimal performance. The fact that both apparatus are cooled to their respective optimal temperature ranges does not imply that the present invention reads on Lipson or for that matter any other cooled apparatus.

- 10.6. If Lipson results in a Fusion reaction the neutrons emitted would be available at a time after it has utility in creating cavitation as in the present invention.

The applicant submits therefore that claims 34-40, 42, 44 and 45 are not anticipated by Lipson. The applicant respectfully submits that this claim should therefore be allowed.

35USC 103 Rejections

11. The examiner states in support of rejection of claim 41:

Claim 41 is rejected under 35 U.S.C. 103(a) as being unpatentable over either one of Margulis or Lipson et al. The size of the bubble is a parameter that depends upon specific design constraints for the system, e.g., the desired energy density of the bubbles (see page 5 of the English language translation of Margulis). Thus, it would have been obvious to modify Margulis or Lipson et al. where an application requires the claimed size of the nucleated bubbles. Such modification would have been within the knowledge and capability of one of ordinary skill in the art at the time of the claimed invention.

The applicant respectfully submits that even if it were proper to combine background art where there is no prior art teaching for their combination, no combination of Margulis and Lipson can replicate the present invention as Margulis is *enabled* with gas bubbles inserted into an unrelated liquid and Lipson is *enabled* with a metal vibrator or protrusion in the fluid, *neither of which are required for the present invention*.

Moreover, even if these enablement requirements for Margulis and Lipson were not present, the methods of both Lipson and Margulis use intentionally gas saturated liquids that result in foaming. Such foaming is governed by the ambient pressures that limit bubble size and simply produce more bubbles of the same size. In contrast the present invention utilizes the tensioned state of the liquid to stretch and grow the nuclear particle seeded bubbles to the required sizes. Therefore the conditions of neither Lipson nor Margulis allow for the growth of bubbles.

The applicant respectfully submits that this claim should therefore be allowed.

12. The examiner states in support of rejection of claims 43 and 46:

Claim 43 and 46 are rejected under 35 U.S.C. 103(a) as being unpatentable over either one of Margulis or Lipson et al. in view of Didenko et al. (Nature 418,7/25/02). Margulis or Lipson et al. disclose(s) the applicant's claims except for the organic liquid. Didenko et al. teach that organic liquids are advantageous for processes involving cavitation because of their very low volatility (see page 4, last full paragraph).

Therefore, it would have been obvious to one having ordinary skill in the art at the time the invention was made to modify the method, as disclosed by Margulis or Lipson et al.,

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by the teaching of Didenko et al., to use organic liquids (which have high accommodation coefficients) for the cavitation liquid, to gain the advantages thereof (i.e., low volatility), because such modification is no more than the use of a well known expedient within the art.

The applicant respectfully submits that even if it were proper to combine background art where there is no prior art teaching for their combination, no combination of Margulis and Didenko or Lipson and Didenko anticipate the present invention.

12.1. Margulis is enabled with gas bubbles inserted into an unrelated liquid. Using an organic liquid as recommended by Didenko does not remove the enablement requirement of Margulis.

12.2. Lipson is enabled with a metal vibrator or protrusion in the fluid. Using an organic liquid as recommended by Didenko does not remove the enablement requirement of Lipson.

12.3. Didenko (July 2002) is preceded by the priority dates of the present application and is therefore not an item of background art (or prior art).

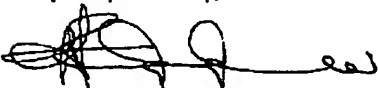
The applicant respectfully submits that these claims should therefore be allowed.

13. The examiner provides a duplicate claim warning with regard to Claim 44 with regard to claim 34. The applicant thanks the examiner for the same and has revised claim 34 in the context of 44 to correct this duplication.

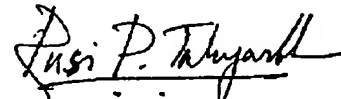
**Conclusion**

The Applicant has amended the claims as required and has provided herewith a response in support of the claims of the present invention. If for any reason this application is not found to be in full condition for allowance, applicant respectfully requests the constructive assistance and suggestions of the Examiner pursuant to M.P.E.P. § 706.03(d) and 707.07(j) in order that the undersigned can place this application in allowable condition as soon as possible and without the need for further proceedings.

Very respectfully,



Dr. Arjuna I. Rajasingham  
Chairman & Chief Executive  
MILLENNIUM ENERGY CORPORATION



Dr. Rusi Taleyarkhan  
Applicant

Att:

1. Replacement paragraphs marked up claims
2. Affidavit under 37CFR 132 – Dr. Xu
3. Affidavit under 37CFR 132 – Dr. Forringer
4. Affidavit under 37CFR 132 – Dr. Bugg
5. " Modeling Analysis and prediction of neutron emission spectra from acoustic cavitation bubble fusion experiments" Nuclear Engineering and Design 238 (20082779-2791)

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**Claims:**

1.(Withdrawn). A nuclear fusion reactor, comprising: a) a reactor chamber for holding a working liquid molecules, said working liquid molecules including at least two nuclei of heavy isotopes of hydrogen; b) structure for placing at least a portion of said liquid into a tension state, said tension state being below a cavitation threshold of said liquid, said tension state imparting stored energy into said liquid portion; c) a nuclear cavitation initiation source for nucleation of at least one bubble from said tension liquid, said bubble having as an nucleated bubble radius being greater than a critical bubble radius of said liquid; d) a pressure field source of growing said as nucleated bubble to form at least one expanded bubble; and e) a pressure field for imploding said expanded bubble, wherein following implosion of said expanded bubble a resulting temperature sufficient to induce at least one nuclear fusion reaction is provided to said liquid.

2(Withdrawn) The reactor of claim 1, wherein said structure for placing said liquid under tension comprises and acoustical wave source.

3 (Withdrawn) The reactor of claim 1, wherein said structure for placing said liquid under tension comprises an acoustical wave source.

4. (Withdrawn) The reactor of claim 2, wherein said acoustical wave source includes an acoustical wave focusing device.

5.(Withdrawn) The reactor of claim 1, wherein said structure for placing said liquid under tension comprises at least one centrifugal source.

6(Withdrawn) The reactor of claim 1, wherein said structure for placing said liquid under tension comprises at least one magnetostrictive source.

7(Withdrawn) The reactor of claim 1, wherein said structure for placing said liquid under tension comprises at least one piezoelectric source.

8(Withdrawn) The reactor of claim 1, wherein said nucleated bubble radius is less than 100 nm.

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9 (Withdrawn) The reactor of claim 1, wherein a ratio of a maximum radius of said expanded bubbles divided by said nucleated bubble radius is at least 105.

10 (Withdrawn) The reactor of claim 1, wherein said nuclear source comprises at least one selected from the group consisting of alpha emitters, neutron sources and fission fragments.

11 (Withdrawn) The reactor of claim 1, wherein said nuclear source comprises a neutron source.

12 (Withdrawn). The reactor of claim 11, wherein said neutron source is an isotopic source having at least one shutter, said shutter opened to synchronize neutron impact with location in said liquid when said liquid is at a predetermined liquid tension level.

13 (Withdrawn) The reactor of claim 1, wherein said nuclear source comprises an alpha particle source.

14 (Withdrawn) The reactor of claim 13, wherein said alpha particle source is dissolved in said liquid.

15 (Withdrawn) The reactor of claim 1, wherein said liquid comprises deuterated acetone.

16 (Withdrawn) The reactor of claim 1, wherein said reactor further includes a controller for synchronizing delivery of at least one cavitation signal from said cavitation initiation source at a predetermined location in said liquid.

17 (Withdrawn) The reactor of claim 1, further comprising a structure for cooling said liquid to a temperature below an ambient temperature.

18 (Withdrawn) The reactor of claim 1, wherein said fusion reaction generates at least one of tritium and neutrons.

19 (Withdrawn) The reactor of claim 1, further comprising at least one external constraint for restraining said liquid.

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20 (Withdrawn) A nuclear fusion-based electrical power plant, comprising: a) a reactor chamber for holding a working liquid; said working liquid molecules including at least two nuclei of heavy isotopes of hydrogen; b) structure for placing at least a portion of said working liquid into a tension state, said tension state being below a cavitation threshold of said liquid, said tension state imparting stored energy into said liquid portion; c) a nuclear cavitation initiation source for nucleation of at least one bubble from said tension liquid, said bubble having an as nucleated bubble radius being greater than a critical bubble radius of said liquid; d) a pressure field source for growing said as nucleated bubble to form at least one expanded bubble; e) a pressure field for imploding said expanded bubble, wherein following implosion of said bubble a resulting temperature sufficient to induce at least one nuclear fusion reaction is provided to said liquid, and f) structure for converting energy released from said fusion reaction to electrical energy.

21. (Withdrawn) A nuclear fusion-based projectile launcher, comprising: a) a reactor chamber for holding a working liquid molecules, said working liquid molecules including at least two nuclei of heavy isotopes of hydrogen; b) structure for placing at least a portion of said working liquid into a tension state, said tension state being below a cavitation threshold of said liquid, said tension state imparting stored energy into said liquid portion; c) a nuclear cavitation initiation source for nucleation of at least one bubble from said tensioned liquid, said bubbles having an as nucleated bubble radius being greater than a critical bubble radius of said liquid; said bubbles a resulting temperature sufficient to induce at least one nuclear fusion reaction is provided to said liquid, and d) a movable constraint bounding said reaction chamber for transferring energy from said fusion reaction to propel a projectile. e) a pressure field for imploding said expanded bubble, wherein following implosion of said bubble a resulting temperature sufficient to induce at least one nuclear fusion reaction is provided to said liquid, and f) a movable constraint bounding said reaction chamber for transferring energy from said fusion reaction to propel a projectile.

22. (Cancelled) A method for producing nuclear fusion, comprising the steps of: a) placing working liquid molecules into a tension state, said working liquid molecules including at least two nuclei of heavy isotopes of hydrogen, said tension state being below the cavitation threshold of said working liquid, said tension state imparting stored energy into said working liquid; b) cavitating at least a portion of said tensioned liquid with nuclear particles sufficient to bubble nucleate at least one bubble, said bubble

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having an as nucleated bubble radius greater than a critical bubble radius of said liquid; c) growing said as nucleated bubble to form at least one expanded bubble using a pressure field; and d) imploding said expanded bubble, wherein a resulting temperature from said implosion is sufficient to induce a nuclear fusion reaction involving said liquid.

23. (Cancelled). The method of claim 22, wherein said fusion reaction is a D-D reaction or a D-T reaction.

24. (Cancelled). The method of claim 22, further comprising the step of degassing said liquid.

25. (Cancelled). The method of claim 22, further comprising the step of cooling said liquid to a temperature below an ambient temperature.

26. (Withdrawn) The method of claim 22, wherein a centrifugal source is used for said tensioning.

27 (Cancelled). The method of claim 22, wherein an acoustical wave source is used for said tensioning.

28 (Cancelled). The method of claim 27, further comprising the step of focusing acoustical waves provided by said acoustical wave source.

29 (Cancelled). The method of claim 22, wherein said as nucleated bubble radius is less than 100 nm.

30 (Cancelled). The method of claim 22, wherein a ratio of a maximum radius of said expanded bubbles divided by said as nucleated bubble radius is at least 105.

31 (Cancelled). The method of claim 22, wherein a neutron source is used for generating neutrons, further comprising the step of synchronizing neutron impact with a location in said working liquid having a predetermined liquid tension level.

32 (Cancelled). The method of claim 22, further comprising the step of synchronizing delivery of at least one cavitation initiation signal with a desired tension level in said liquid.

33 (Cancelled). The method of claim 23, wherein said liquid comprises deuterated acetone.

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34. (Currently amended). A method for producing thermonuclear nuclear fusion, comprising the steps of: providing a working liquid enriched with molecules comprising isotopic D or T atoms ~~comprising molecules~~; placing at least a portion of said liquid into a tension state, a maximum tension in said tension state being below the cavitation threshold of said liquid, said tension state imparting stored mechanical energy into said liquid portion; directing fundamental particles ~~nucleating agents comprising at least one of: neutrons, photons, alpha particles and fission products~~, at said liquid portion when said liquid portion is in said tension state, said nucleating agents having sufficient energy for nucleating a plurality of bubbles substantially filled with vapor from said liquid, said bubbles substantially filled with vapor having an as nucleated bubble radius greater than a critical bubble radius of said liquid; growing said bubbles; and imploding said bubbles substantially filled with vapor, wherein a resulting temperature obtained from energy released from said implosion is sufficient to induce a nuclear fusion reaction of said isotopic D or T atom comprising molecules in said liquid portion.

35. (Previously presented). The method of claim 34, wherein said thermonuclear fusion reaction is a D-D reaction or a D-T reaction.

36. (Previously presented). The method of claim 34, further comprising the step of cooling said liquid to a temperature below an ambient temperature.

37. (Previously presented). The method of claim 34, wherein said tension state is a part of a time-varying pressure state including compressive and tensile portions.

38. (Previously presented). The method of claim 34, wherein said tension state is a constant tension state.

39. (Previously presented). The method of claim 34, wherein an acoustical wave source is used for said tensioning.

40. (Previously presented). The method of claim 39, further comprising the step of focusing acoustical waves provided by said acoustical wave source.



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41. (Previously presented). The method of claim 34, wherein said nucleated bubble radius is from 10 to 100 nm.
42. (Previously presented). The method of claim 34, wherein a neutron source is used for said nucleating, further comprising the step of synchronizing neutron impact with a location in said liquid having a predetermined liquid tension level.
43. (Previously presented). The method of claim 34, wherein said liquid is an organic liquid.
44. (Previously presented). The method of claim 34, wherein said fundamental particles are selected from the group consisting of alpha particles, neutrons and fission fragments.
45. (Previously presented). The method of claim 34, wherein said growing and imploding occurs responsive to an applied acoustical field.
46. (Previously presented). The method of claim 34, wherein said liquid is a high accommodation coefficient liquid.
47. (currently amended) A method ~~An apparatus~~ for producing thermonuclear fusion, comprising the steps of : filling a chamber with ~~containing~~ a high accommodation coefficient liquid; ~~a means for~~ inducing tension in said high accommodation coefficient liquid; directing a nucleating agent comprising at least one of: neutrons, alpha particles, photons and fission products to said chamber; ~~a means for~~ enhancing the size of the nucleated bubbles in tension to a volume greater than a predetermined volume before inducing controlled implosion; thereby producing thermonuclear fusion.
48. (new) A method of claim 34, wherein the working liquid is de-gassed prior to being put in a tension state.

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Statement of Dr. Yiban Xu

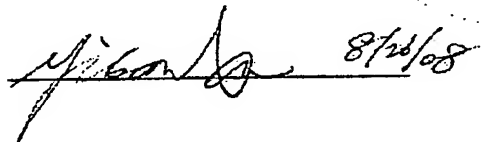
This affidavit is being supplied to state that if called upon, I, Yiban Xu would be competent to confirm as to the accuracy of the following in relation to the experiments on bubble (sono) fusion that I have conducted or participated in:

1. I am making this statement of my own personal knowledge and of my own free will. All of the facts contained in this statement are true.
2. I obtained my PhD in Nuclear Engineering in 2004 and reside in Lafayette, IN, USA.
3. The bubble fusion test cell apparatus used for my confirmatory studies (Xu et al., 2005) was based on the design used by the Taleyarkhan et al. team as reported in their published papers (Taleyarkhan et al., 2002; Taleyarkhan et al., 2004; Taleyarkhan et al., 2006).
4. There was no intentional effort to dissolve gases into the test liquid prior to conducting bubble fusion experiments.
5. Control experiments were conducted to ensure that bubble fusion signals (neutrons and/or tritium) were generated only when the test liquid was deuterated, and when it was undergoing nuclear particle based cavitation.
6. There was no acoustic horn or such vibrator that was dipped into the test liquid during conduct of my reported bubble fusion experiments. In my bubble fusion experiments of the type reported by Taleyarkhan et al. the nucleation of bubbles occurs away from solid-liquid interfaces. Acoustic energy was provided into the test liquid by use of a piezo-electric element epoxied to the outside of the glass wall.
7. In the experiments that I was involved, care was taken to ensure that there were no extraneous sources of nuclear particles that could have given rise to the bubble fusion signatures as reported for my experiments and studies (Xu et al., 2005).
8. The pressure distribution of the bubble fusion test cell (as used for my studies based on the Taleyarkhan et al., 2002 design) produces neutron sensitive cavitation regions away from the solid-liquid interfaces. This is due to the pressure profiles which ensure that bubble nucleation takes place within the bulk of the liquid once the input power is increased above a certain level readily determined experimentally. This attribute is a consequence of the pressure profiles in such a design which is an aspect that I have confirmed for myself while conducting oscillating pressure mapping tests also.

References Cited Above:

- Taleyarkhan, R. P., et al., Science, 295, 1868, 2002.
- Taleyarkhan, R.P., et al., Phys. Rev. E, 69, 2004.
- Taleyarkhan, R.P., et al., Phys. Rev. Ltrs., 96, 034301, 2006.
- Xu, Y., and A. Butt, Nucl. Eng. Design, 235, 1317-1324, 2005.
- Xu, Y., A. Butt and S. Revankar, Proc. 11<sup>th</sup> Int. Conf. Nuclear Reactor Thermal-Hydraulics, NURETH-11, France, 2005.

Signed:



Affidavit of Dr. JaeSeon Cho

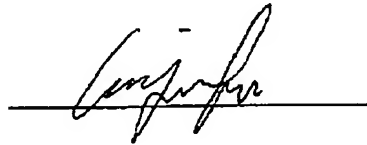
This affidavit is being supplied to state that if called upon, I, JaeSeon Cho would be competent to confirm as to the accuracy of the following in relation to the experiments on bubble (sono) fusion that I have conducted or participated in:

1. I am making this statement of my own personal knowledge and of my own free will. All of the facts contained in this statement are true.
2. I obtained my PhD in Nuclear Engineering in 1999 from Seoul National University and I currently work for FNC Tech. Inc., a high-technology company in S. Korea where I reside.
3. The bubble fusion test cell apparatus used for my studies was based on the design used by the Taleyarkhan et al. team as reported in their published papers (Taleyarkhan et al., 2002; Taleyarkhan et al., 2004; Taleyarkhan et al., 2006). This is true also for the apparatus in my paper (Cho et al., 2003).
4. There was no intentional effort to dissolve gases into the test liquid prior to conducting bubble fusion experiments.
5. Control experiments were conducted to ensure that bubble fusion signals (neutrons and/or tritium) were generated only when the test liquid was deuterated, and when it was undergoing nuclear particle based cavitation.
6. There was no acoustic horn or such vibrator that was dipped into the test liquid during conduct of my reported bubble fusion experiments. In my bubble fusion experiments of the type reported by Taleyarkhan et al. the nucleation of bubbles occurs away from solid-liquid interfaces. Acoustic energy was provided into the test liquid by use of a piezo-electric element epoxied to the outside of the glass wall.
7. In the experiments that I was involved, care was taken to ensure that there were no extraneous sources of nuclear particles that could have given rise to the bubble fusion signatures as reported for my experiments and studies.
8. The pressure distribution of the bubble fusion test cell as used for my studies (Cho et al., 2004) was based on the Taleyarkhan et al., 2002 design. It produces neutron sensitive regions away from the solid-liquid interfaces. This is due to the induced pressure profiles, which ensure that bubble nucleation takes place within the bulk of the liquid. This attribute is a consequence of the pressure profiles in such a design which is an aspect that I have confirmed for myself while conducting oscillating pressure mapping tests (see Figs. 2 and 6 of Cho et al., 2004). The threshold pressure for neutron based nucleation is readily determined by increasing acoustic power to the point where nuclear particle based cavitation begins.

References Cited Above:

- Cho, J. S., & R. P. Taleyarkhan, Proc. 10<sup>th</sup> Int. Conf. Nucl. Reac. Thermal Hydraulics, Seoul, S. Korea, October 5-9, 2003.
- Taleyarkhan, R. P., et al., Science, 295, 1868, 2002.
- Taleyarkhan, R. P., et al., Phys. Rev. E, 69, 2004.
- Taleyarkhan, R. P., et al., Phys. Rev. Lett., 96, 034301, 2006.

Signed:



**Affidavit of Professor William Bugg**

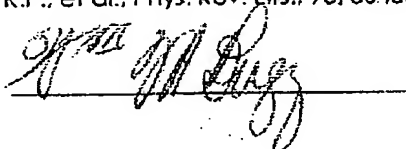
This affidavit is being supplied to state that if called upon, I, William Bugg would be competent to testify as to the accuracy of the following in relation to the experiments and studies on bubble (sono) fusion that I have conducted or participated in:

1. I am making this affidavit of my own personal knowledge and of my own free will. All of the facts contained in this affidavit are true.
2. I obtained my PhD in 1959 from the University of Tennessee-Knoxville, where I served as Head of Physics from 1969 to 1996. I am a Fellow of the American Physical Society and am currently a scientific researcher at Stanford University's SLAC facility.
3. The bubble fusion test cell apparatus used for the confirmatory studies I was involved in (Bugg, 2006) was similar to that used by the Taleyarkhan et al. team as reported in their published papers (Taleyarkhan et al., 2002; Taleyarkhan et al., 2004; Taleyarkhan et al., 2006).
4. There was no intentional effort to dissolve gases into the test liquid prior to conducting bubble fusion experiments. On the contrary the containers were initially pumped to remove gases.
5. Control experiments were conducted to ensure that bubble fusion signals (neutrons and/or tritium) were generated only when the test liquid was deuterated, and when it was undergoing nuclear particle based cavitation.
6. There was no acoustic horn or such vibrator that was dipped into the test liquid during conduct of my bubble fusion experiments. In my bubble fusion experiments of the type reported by Taleyarkhan et al. the nucleation of bubbles occurs away from solid-liquid interfaces. Acoustic energy was provided into the test liquid by use of a piezo-electric element epoxied to the outside of the glass wall.
7. In the experiments that I was involved in, I carefully ensured the absence of external sources of neutrons (such as Californium) that could have given rise to the bubble fusion neutron emission signatures as documented in my report (Bugg, 2006).
8. For the bubble fusion confirmatory experiments that I participated in, I noted that spherically-shaped bubbles formed and imploded within the bulk of the liquid away from the walls of containers.

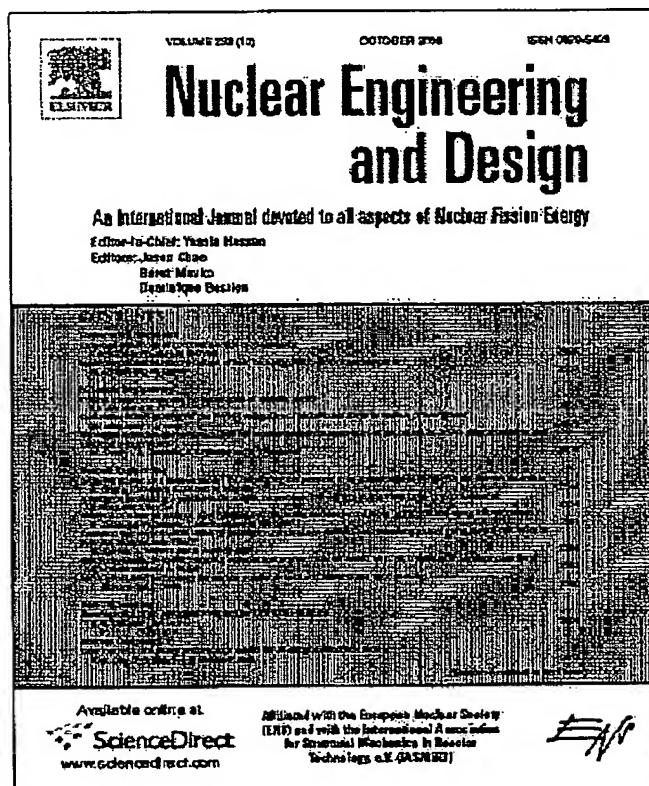
**References Cited Above:**

- Bugg, W., "Report on Activities on June 6-7 Visit.." Report to Purdue University via email attachment, June 9, 2006.
- Taleyarkhan, R. P., et al., Science, 295, 1868, 2002.
- Taleyarkhan, R.P., et al., Phys. Rev. E, 69, 2004.
- Taleyarkhan, R.P., et al., Phys. Rev. Ltrs., 96, 034301, 2006.

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## Modeling, analysis and prediction of neutron emission spectra from acoustic cavitation bubble fusion experiments

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### ABSTRACT

Self-nucleated and external neutron nucleated acoustic (bubble fusion) cavitation experiments have been modeled and analyzed for neutron spectral characteristics at the detector locations for all separate successful published bubble fusion studies. Our predictive approach was first calibrated and validated against the measured neutron spectrum emitted from a spontaneous fission source (<sup>252</sup>Cf), from a Pu–Be source and from an accelerator-based monoenergetic 14.1 MeV neutrons, respectively. Three-dimensional Monte-Carlo neutron transport calculations of 2.45 MeV neutrons from imploding bubbles were conducted, using the well-known MCNP5 transport code, for the published original experimental studies of Taleyarkhan et al. [Taleyarkhan, et al., 2002. *Science* 295, 1868; Taleyarkhan, et al., 2004. *Phys. Rev. E* 69, 036109; Taleyarkhan, et al., 2006a. *PRL* 96, 034301; Taleyarkhan, et al., 2006b. *PRL* 97, 149404] as also the successful confirmation studies of Xu et al. [Xu, Y., et al., 2005. *Nuclear Eng. Des.* 235, 1317–1324], Forringer et al. [Forringer, E., et al., 2006a. *Transaction on American Nuclear Society Conference*; vol. 95, Albuquerque, NM, USA, November 15, 2006, p. 736; Forringer, E., et al., 2006b. *Proceedings of the International Conference on Fusion Energy*, Albuquerque, NM, USA, November 14, 2006] and Bugg [Bugg, W., 2006. *Report on Activities on June 2006 Visit*, Report to Purdue University, June 9, 2006]. NE-213 liquid scintillation (LS) detector response was calculated using the SCINFUL code. These were cross-checked using a separate independent approach involving weighting and convoluting MCNP5 predictions with published experimentally measured NE-213 detector neutron response curves for monoenergetic neutrons at various energies. The impact of neutron pulse-pileup during bubble fusion was verified and estimated with pulsed neutron generator based experiments and first-principle calculations. Results of modeling-cum-experimentation were found to be consistent with published experimentally observed neutron spectra for 2.45 MeV neutron emissions during acoustic cavitation (bubble) fusion experimental conditions with and without ice-pack (thermal) shielding. Calculated neutron spectra with the inclusion of ice-pack shielding are consistent with the published spectra from experiments of Taleyarkhan et al. [Taleyarkhan, et al., 2006a. *PRL* 96, 034301] and Xu et al. [Xu, Y., et al., 2005. *Nuclear Eng. Des.* 235, 1317–1324] where ice-pack shielding was present, whereas without ice-pack shielding the calculated neutron spectrum is consistent with the experimentally observed neutron spectra of Taleyarkhan et al. [Taleyarkhan, et al., 2002. *Science* 295, 1868; Taleyarkhan, et al., 2004. *Phys. Rev. E* 69, 036109] and Forringer et al. [Forringer, E., et al., 2006a. *Transaction on American Nuclear Society Conference*, vol. 95, Albuquerque, NM, USA, November 15, 2006, p. 736; Forringer, E., et al., 2006b. *Proceedings of the International Conference on Fusion Energy*, Albuquerque, NM, USA, November 14, 2006] and also that from GEANT computer code [Agostinelli, S., et al., 2003. *Nuclear Instrum. Methods Phys. Res. A* 506, 250–303] predictions [Naranjo, B., 2006. *PRL* 97 (October), 149403], in which ice shielding was also absent.

The results of this archive confirm for the record that the confusion and controversies caused from past reports [Reich, E., 2006. *Nature* (March) 060306. [news@nature.com](mailto:news@nature.com); Naranjo, B., 2006. *PRL* 97

Abbreviations: Cf, californium; Cl, Curie; D, deuterium; GEANT, a Monte-Carlo nuclear particle interaction code system; n, neutron; MCNP, Monte-Carlo N-particle computer code; NE-213, trademark of scintillation liquid from Nuclear Enterprises Inc.; LS, liquid scintillation; PNG, pulse neutron generator; PRE, proton recoil edge; PSD, pulse-shape discrimination; Pu–Be, plutonium–beryllium; SCINFUL, scintillator full response computer code; T, tritium; UN, uranyl nitrate;  $\gamma$ , gamma photon.

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(October) 149403] have resulted from their neglect of important details of bubble fusion experiments. Results from this paper demonstrate that ice-pack shielding between the detector and the fusion neutron source, gamma photon leakage and neutron pulse-pileup due to picosecond duration neutron pulse emission effects play important roles in affecting the spectra of neutrons from acoustic inertial confinement thermonuclear fusion experiments.

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## 1. Introduction

In 2006, evidence was presented for a unique, new stand-alone acoustic inertial confinement fusion device that was successfully tested and results published (Taleyarkhan et al., 2006a). Those experiments were conducted with four different liquid types in which bubbles were nucleated without the use of external neutron sources. Four independent detector systems were used [a neutron track plastic detector to provide unambiguous visible records for fast neutrons, a LiI thermal neutron detector, a NE-213-type liquid scintillation (LS) detector, and a NaI gamma ( $\gamma$ ) ray detector]. All detector systems measured statistically significant (from 6 to 20+ standard deviations) nuclear emissions for experiments with deuterated benzene and acetone mixtures but not for experiments with heavy water, a finding which validated theoretical predictions (Nigmatulin et al., 2005) of our simulations of the implosion dynamics which indicated that heavy water would not be a good choice for attaining thermonuclear fusion in imploding bubbles. The measured neutron energies from bubble fusion experiments were, as expected, substantially  $\leq 2.45$  MeV. Control experiments did not result in statistically significant neutron or  $\gamma$  ray emissions. These observations of neutron emissions in self-nucleated experiments with deuterated benzene-acetone mixtures but not for the controls (i.e., non-deuterated mixtures) have been successfully confirmed (Forringer et al., 2006a,b; Bugg, 2006). In the studies of Forringer et al. and Bugg, the experimental configurations they used were different from that used by Taleyarkhan et al. (2006a,b). The two experimental configurations are shown in Fig. 1a and b. As noted therein, a principle distinguishing factor between the two configurations is the presence or absence of  $\sim 3$  cm of ice-pack materials acting as thermal shielding around the test cell enclosure. Whereas, in the reported experimental systems of Taleyarkhan et al. (2002, 2004, 2006a,b) the ice-pack shielding was required and present, the same was not true in the experiments conducted by Forringer et al. (2006a,b) and Bugg (2006).

The results of Taleyarkhan et al. (2006a) using the LS detector system offered the highest level of statistical significance of above 17 standard deviations (S.D.). Because of the presence of intervening ice-pack shielding, the published neutron spectrum (Taleyarkhan et al., 2006a) incorporated characteristics that were different from the shape of the neutron spectrum for a monoenergetic 2.45 MeV neutron emanating from the test cell without having to interact with ice-pack shielding. A qualitative discussion was provided (Taleyarkhan et al., 2006b) in response to questions and comments raised from code calculations for the presumed geometric configuration by Naranjo (2006) of the University of California at Los Angeles (UCLA). Unfortunately, the UCLA predictions were made for an incorrectly presumed experimental configuration (e.g., with no ice-packs) and would actually be more applicable for comparisons with the published measured neutron spectra of Forringer et al. (2006a,b) and Taleyarkhan et al. (2002, 2004) rather than those of Taleyarkhan et al. (2006a). Nevertheless, these faulty simulations seeded and caused considerable controversy and confusion (Reich, 2006; Naranjo, 2006).

In 2002 and 2004, evidence was first presented for the neutron spectrum measured during external neutron-based acoustic cavitation experiments (Taleyarkhan et al., 2002, 2004). In these

experiments nucleation of bubbles in pure deuterated acetone ( $C_3D_8O$ ) was achieved using a 14.1 MeV pulse neutron generator (PNG). The test geometry for this study is shown in Fig. 1d. Although the enclosure is similar to that for Fig. 1a, the LS detector was positioned to be within the enclosure as shown with no intervening ice-pack materials. The results of the 2004 studies reported by Taleyarkhan et al. (2004) were successfully confirmed in studies reported by Xu et al. (2005) in which they used a different experimental enclosure type as shown in Fig. 1c, and the bubble nucleation was conducted using randomly emitted neutrons from an isotope source. However, as for the self-nucleation bubble fusion reports of Taleyarkhan et al. (2005a,b), in the Xu et al. (2005) studies, their LS detector was also positioned outside the freezer, and as such, a  $\sim 3$ –4 cm of ice layer was also present between the test cell and the LS detector.

The purpose of this paper is to present a comprehensive unifying study for all the reported successful bubble fusion studies with the goal to remedy the unfortunate controversies and confusion resulting from the misguided simulations for incorrect experimental configurations as reported in the literature (Reich, 2006; Naranjo, 2006), as well as due to the omission of important effects such as pulse-pileup and gamma photon leakage. For completeness, we have conducted simulations of successful published studies not only for the self-nucleation experiments, but also, for the external neutron-based experiments.

Questions have also been raised (Reich, 2006) concerning the detection of neutron counts in channels higher than the 2.45 MeV proton recoil edge (PRE). The present paper includes results of analyses, backed up with experimental evidence, for clarifying the principle mechanisms concerning such occurrence for bubble fusion experiments.

## 2. Two independent modeling-simulation approaches

In order to evaluate the relative effects on the expected 2.45 MeV spectrum with and without ice-pack shielding we conducted assessments with two independent methods to obtain cross-checks and better confidence for the validity of our predictions. The first approach was to establish a simulation platform similar to that used by UCLA in which results of three-dimensional neutron transport from within the test cell were derived using the USDOE's code system MCNP5 (MCNP, 2003) at the location of the LS detector. This down scattered neutron flux profile was next combined with the USDOE's *Scintillator Full* (SCINFUL) response Monte-Carlo based code system (Dickens, 1988). SCINFUL was developed specifically for predicting the response function of neutron interactions with NE-213 detectors. The second approach we developed was to act as a cross-check to the MCNP5-SCINFUL predictions. It involves directly combining the neutron emission spectra emanating from the experimental system (as derived from MCNP5 simulations) with the published (i.e., directly measured) neutron energy-related pulse-height spectra for an actual 5 cm  $\times$  5 cm sized NE-213 detector (viz., of the same size and type as used by Taleyarkhan et al., 2002, 2004, 2006a,b; Xu et al., 2005; also by Forringer et al., 2005a,b). Predictions from both approaches could then be compared with the various published bubble fusion experimental data.

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## 2.1. Calibration-benchmarking of LS detector with prediction methodology

The SCINFUL code requires the user to provide to it the incoming neutron energy spectrum (e.g., from a known source of neutrons of various energies). A known source could be from a National Institute of Standards and Technology (NIST)-certified isotope source or from an accelerator-based system. Alternately, it could be the prediction from a well-characterized nuclear particle transport code such as MCNP5. SCINFUL utilizes Monte-Carlo techniques and has itself been extensively benchmarked by the developers against a variety of experimental databases for its ability to predict the overall response of a NE-213 LS detector system to incoming neutrons over the energy range 0.5–80 MeV. A known shortcoming is associated with the PRE where detector resolution issues can lead to smearing-related extension of counts to higher channels

In an actual detector system but this is not possible to model theoretically since it involves intricacies of individual detector construction and multidimensional issues. In order to gain confidence in the prediction methodology employed for this study it was decided to ourselves calibrate the SCINFUL code predictions for our laboratory's 5 cm × 5 cm NE-213 LS detector using the electronic component train and settings for the published bubble fusion experimental spectra. The comparisons were made for three different neutron sources. The first two were NIST-certified isotope-based neutron-gamma sources: (1) 1 Ci, Pu–Be source emitting  $\sim 2 \times 10^6$  n/s; (2)  $\sim 0.1$  mCi,  $^{252}\text{Cf}$  source emitting  $\sim 10^5$  n/s. The second type of neutron source produced 14.1 MeV monoenergetic neutrons from an accelerator device commonly called a PNG and is based on D–T interactions. The emission rate was about  $5 \times 10^5$  n/s. The NE-213 LS detector was placed  $\sim 30$  cm from each of these sources and the spectra were obtained with and without

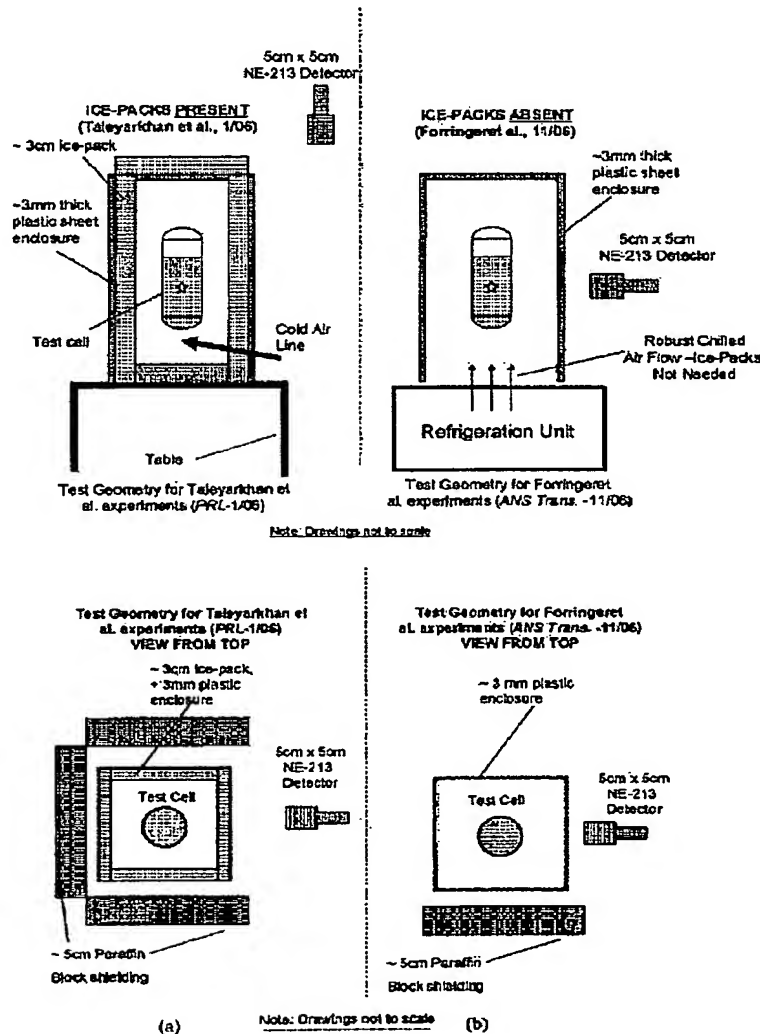


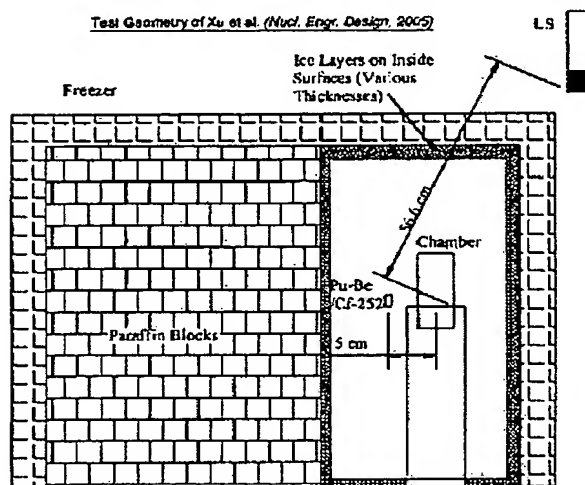
Fig. 1. Experimental geometries of (a) Taleyarkhan et al. (2006a,b) (b) Forringer et al. (2006a,b) (c) Xu et al. (2006) and (d) Taleyarkhan et al. (2002, 2004).



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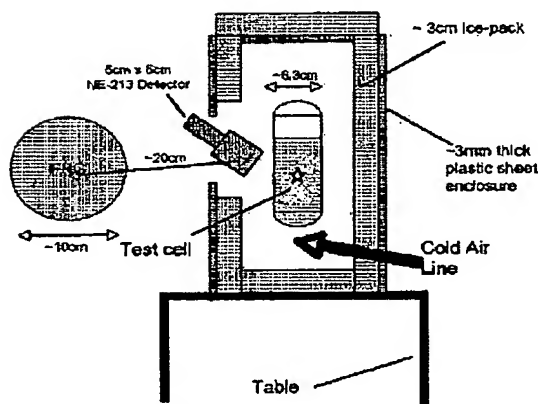
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(1c) – Xu et al. (2005)

Test Geometry for Taleyarkhan et al. (Science 3/2002; Phys. Rev. E-3/2004)



Notes: (1) Drawing not to scale  
(2) Paraffin shielding around enclosure is not shown

(1d) – Taleyarkhan et al. (2002, 2004)

Fig. 1. (Continued).

pulse-shape discrimination (PSD). PSD permits rejection of gamma photon-based detector counts from those caused from neutron interactions. At the PSD settings used for the published studies (Taleyarkhan et al., 2002, 2004, 2006a,b; Xu et al., 2005; Forringer et al., 2006a,b) it is estimated that roughly 95% of gamma photons are rejected. Fig. 2a shows the relative spectral emissions for each of these three emission types. Results of the measurements for each of these three sources with and without PSD are shown in Fig. 2b. As noted from Fig. 2b, the monoenergetic 14.1 MeV neutron spectrum displays a sharp reduction in counts at the 14.1 MeV PRE region (channel ~175) but counts still persist and leak into higher channels due to imperfect detector resolution. Since a 14.1 MeV-T accelerator does not generate gamma photons, the vast majority of counts are neutron driven. For a Pu-Be source, as noted from Fig. 2a,

the neutron energies are not monoenergetic but spread out over a large range (0.1 MeV–~10 MeV; the average energy is in the 4 MeV range with a tail towards 11 MeV at which the intensity drops close to zero. Importantly, a Pu-Be source also emits a strong 4.4 MeV gamma photon (Knolls, 1999), roughly at the same rate as for neutron emission; however, unlike the neutrons which are spread out in energy, the gamma photon is monoenergetic due to which, per expectations, we note in Fig. 2b a noticeable jump in the combined neutron-gamma (i.e., without PSD) spectrum around channel 90. As is also seen from Fig. 2a, for the  $^{252}\text{Cf}$  isotope-based source, the neutrons are emitted from spontaneous fission with a peak intensity at ~0.8 MeV, with an average spectrum energy of ~1.98 MeV, and with a long tail extending through ~12 MeV where the intensity drops close to zero.  $^{252}\text{Cf}$  also emits about three times more

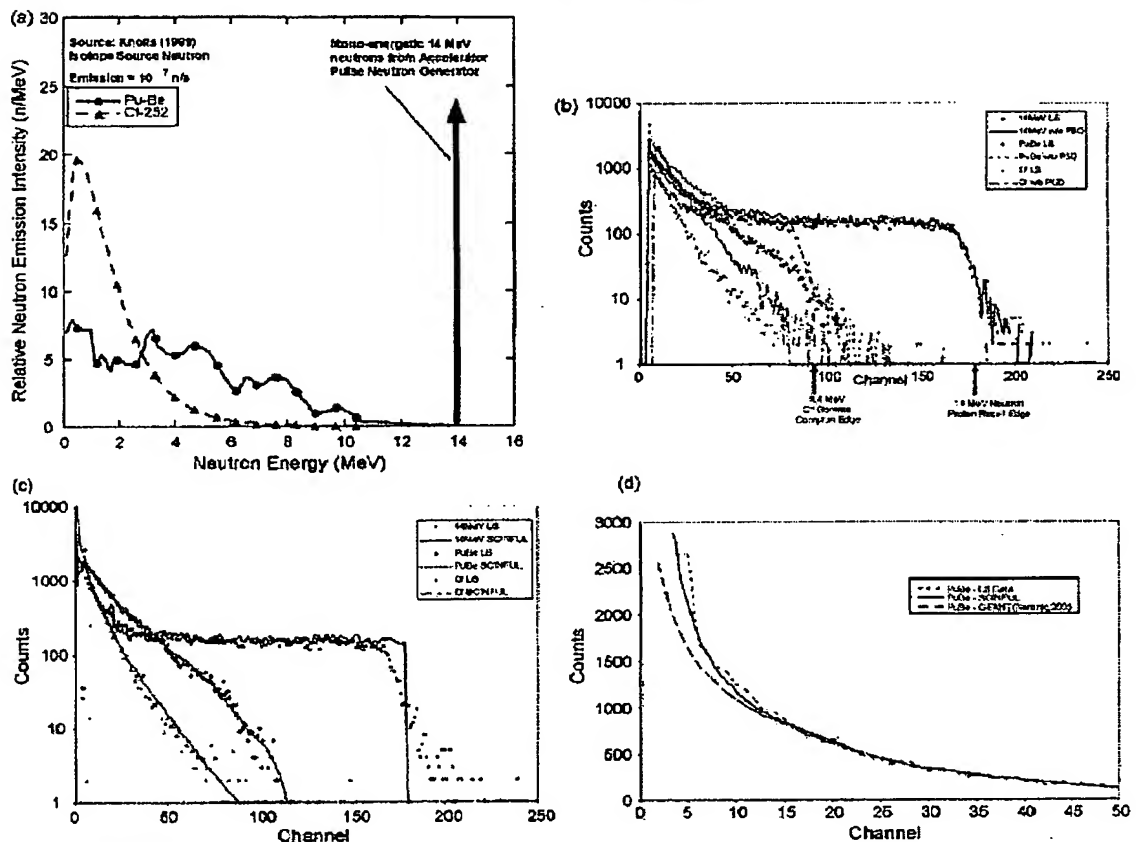


Fig. 2. (a) Spectral shapes of neutron emission intensity vs. energy for various sources used for calibration studies. (b) Measured pulse-height neutron-gamma spectra using 5 cm × 5 cm NE-213 LS Detector with (symbols) and without (lines) pulse-shape-discrimination (PSD) with isotope (<sup>252</sup>Cf, Pu-Be) and 14 MeV monoenergetic neutron from PNG. (c) SCINFUL code predictions vs. measured neutron spectra with 5 cm × 5 cm NE-213 LS detector (with PSD). (d) SCINFUL and GEANT code predictions vs. measured neutron spectrum from a Pu-Be neutron source using a 5 cm × 5 cm NE-213 LS Detector. Note: Under predictions at lower channels are more pronounced for GEANT calculations—a feature which has also been reported by Patronis et al. (2007).

gamma photons (Knolls, 1999) for each neutron emission and we see this in the measured spectrum of Fig. 2b.

The 14.1 MeV neutron energy and published neutron spectra for the <sup>252</sup>Cf and Pu-Be sources were entered as input for SCINFUL code predictions of response for a 5 cm × 5 cm NE-213 detector. This is similar to what one would undertake to do if one were to rely on simulations (e.g., from MCNP5 predictions of down scattered neutron spectra). Results of SCINFUL code predictions for each of the three neutron sources are shown in Fig. 2c alongside the measured LS detector spectra with PSD. As noted therein, the SCINFUL code predictions capture the overall neutron spectral shapes for all three sources with excellent correlation over the entire energy range of ~0.5 MeV at the lower-level cutoff, to ~14 MeV, for the monoenergetic 14.1 MeV neutron spectrum. The coefficient for determination (so-called  $R^2 = 1 - SS_{\text{err}}/SS_{\text{tot}}$ ; where  $SS_{\text{err}}$  is the regression sum of squares, and  $SS_{\text{tot}}$  is the total sum of squares proportional to the sample variance) ranged from ~91% to ~98%. Around the PRE channel (~175) SCINFUL predicts a sharp (almost vertical) rise in counts indicating the response to a head-on collision of the 14.1 MeV neutron with protons in the LS detector liquid. The measured spectrum also shows a significant rise in counts but the shape of this measured spectrum is somewhat smeared as expected for practical

detectors (i.e., slanted at ~45° with counts leaking through to channel 250). Such an effect is well-known (Dickens, 1988; Knolls, 1999; Lee and Lee, 1998). This calibration-cum-benchmarking provides good confidence in the ability to predict the spectral response of a 5 cm × 5 cm NE-213 LS detector using a combination of an arbitrary input spectrum of neutron energies together with the SCINFUL code.

At the lower end of the abscissa corresponding to low-angle scattering of neutrons with protons and carbon atoms, a discrepancy between prediction and measurements may be expected as shown in Fig. 2d for comparisons against the measured Pu-Be neutron source spectrum of Fig. 2a. Also presented in Fig. 2d is the published prediction for a Pu-Be source using another Monte-Carlo based code, viz., GEANT (Agostinelli et al., 2003; Naranjo, 2006). SCINFUL and GEANT both tend to somewhat under predict the measured spectrum with the under prediction being greater for the GEANT code simulation as has also been reported elsewhere in the literature for GEANT (Patronis et al., 2007). However, except for some under prediction at lower channels, for most of the energy scale through the PRE channels and beyond, both SCINFUL and GEANT appear to be well-suited for predicting the measured neutron response spectrum for the NE-213 LS detector.

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It is also well-known and documented for the SCINFUL code (Dickens, 1988) that detector resolution will vary from detector to detector depending on numerous factors such as light collection efficiency at liquid–photomultiplier interface, age of the detector, etc. Models of detector response for neutron-induced proton recoils therefore, usually model the detector as being one of perfect resolution—which then leads to a sharp increase at the PRE and no counts beyond the PRE (whereas, in actuality a sloping shoulder will be present and counts will occur in channels far beyond the PRE channel number). The capturing of such an effect is at times attempted by Monte-Carlo codes by artificially including a so-called resolution function (see for example, Dickens, 1988) for a given practical detector to force-fit the code predictions at the PRE location to the actual data profile against which it is to be compared in the first instance. Nevertheless, even without engaging in such artifacts, as also demonstrated with our own calibration in this section, the combined MCNP5–SCINFUL code system offers an excellent tool for predicting and studying the essential characteristics of the expected pulse-height spectrum for our experiments for the bulk of the pulse-height spectrum (i.e., for channels below the PRE).

### 3. Modeling approaches for comparing predictions with measured spectra from acoustic inertial confinement (bubble) fusion experiments

The calibrated SCINFUL code approach which was just discussed was next used to predict the LS detector neutron pulse-height spectrum for comparison against the published spectra. However, instead of using the well-established (i.e., known) neutron energy and spectrum of neutrons from an isotopic or PNG source, the neutron energy spectrum has now to be calculated. A D–D thermonuclear fusion event produces a 2.45 MeV neutron. In a typical bubble fusion experiment, this 2.45 MeV neutron is produced within a deuterated liquid contained in a test cell of approximately 3 cm in radius. Before reaching the LS detector this fusion neutron would necessarily become down scattered in energy as it interacts with intervening atoms of the test liquid, the container wall and shielding materials. It is this downscattered neutron energy spectrum which becomes the source input for SCINFUL predictions of the LS detector pulse-height response, which thereafter, can be directly compared against published experimental data to note how well the published spectra compare with the predicted values. Good agreement provides validation for the neutron source as being that from a D–D fusion event, in much the same manner as the good agreements of Fig. 2c validated the source of neutrons as being from  $^{252}\text{Cf}$ , Pu–Be and PNG neutron sources, respectively.

#### 3.1. MCNP5–SCINFUL response simulation

Therefore, as a first step, the transport characteristics of a 2.45 MeV neutron through ~3 cm of test cell liquid, followed by the enclosure wall, were computed using the well-known MCNP5 nuclear transport code (MCNP, 2003) developed by the Los Alamos National Laboratory (LANL). A three-dimensional (3D) model for each of the experimental geometries shown in Fig. 1 was developed. The prediction of the emanated spectrum was used as input for SCINFUL predictions as done before in Section 2. This calculational model is referred to as MCNP5–SCINFUL.

#### 3.2. MCNP5–NE-213 response simulation—an alternate independent approach (MCNP5 neutron spectrum combined piece-wise with measured NE-213 detector response for various neutron energies)

A second modeling approach (referred to herein as “MCNP5–NE-213”) was developed to independently compare with the

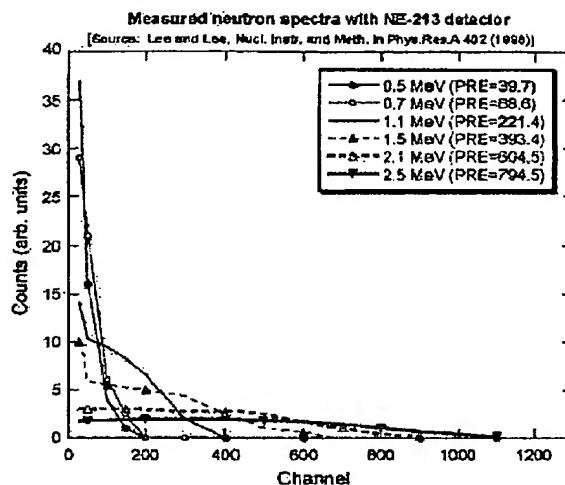


Fig. 3. Measured pulse-height spectra in a 5 cm × 5 cm NE-213 detector (Lee and Lee, 1998) for neutron energies ranging from 0.5 to 2.5 MeV. Note: The PRE channel was chosen to be mid-way of the shoulder for each curve (e.g., for 2.5 MeV, the PRE light output channel was deemed to be ~600). Note also that, due to imperfect detector resolution, significant counts occur above the PRE channel.

predictions of the MCNP5–SCINFUL code predictions discussed earlier. This was considered useful for two reasons. First, to cross-check and evaluate that SCINFUL code predictions against experimental data were in line with expectations for the spectrum shape below the 2.45 MeV PRE. The second reason was to help assess how many and how far above the 2.45 MeV PRE one should expect counts due to imperfect detector resolution, a well-known effect (e.g., Dickens, 1988; Lee and Lee, 1998) and also highlighted in established textbooks on the subject (Knolls, 1999). Fortunately, in a relevant study (Lee and Lee, 1998) the authors used a 5 cm × 5 cm NE-213 detector identical in size to the one used in the Taleyarkhan et al. (2002, 2004, 2006a,b), Forringer et al. (2006a,b), and Xu et al. (2005) studies. The Lee and Lee study has published individual pulse-height spectra at six neutron energies ranging from 0.5 MeV to 2.5 MeV. Their results of the measured spectra are replotted in Fig. 3, where the legend for each neutron energy includes the PRE channel number for each of the six neutron energies. As also noted from standard textbooks (Knolls, 1999) we readily note that significant counts can be expected in channel numbers far above the PRE channel for NE-213 type LS detectors. The availability of the six profiles at various neutron energies permits one to combine MCNP5 predictions for incoming neutrons at various energies with these six profiles, thereby acting as a cross-check for the MCNP5–SCINFUL model. That is, instead of relying solely on SCINFUL, we can now also rely on the published experimental response curves at discrete neutron energies of Fig. 3 for an actual detector of the type and size used in the bubble fusion experiments of Taleyarkhan et al. (2002, 2004, 2006a,b), Xu et al. (2005), and Forringer et al. (2006a,b). This model is herein, referred to as the MCNP5–NE-213 model.

However, since MCNP5 predictions for down scattered neutrons are over a continuous energy range, the MCNP5–NE-213 model requires binning. For this reason, the MCNP5 neutron spectrum variation with energy is broken down into six energy groups consistent with the six neutron energies of Fig. 3 to provide the relative proportion of neutrons in each bin. Thereafter, the digitized values of pulse-height spectra of Fig. 3 at each of six energy levels are multiplied by the relative fractional neutron counts (from MCNP5

simulations) in corresponding energy bins and the individual spectra are combined to obtain an overall composite spectrum.

#### 4. Comparison of MCNP5–SCINFUL and MCNP5–NE-213 predictions with self-nucleation and externally nucleated bubble fusion experimental data

Comparison of predictions is shown separately for the self-nucleation experiments and then for the external neutron-based bubble fusion experiments. The more recent self-nucleation experiments are addressed first.

##### 4.1. Comparison with self-nucleated bubble fusion experimental data

In self-nucleated bubble fusion experiments of Taleyarkhan et al. (2006a,b) and Forringer et al. (2006a,b) and Bugg (2006), the nucleation of bubbles was achieved using dissolved uranyl nitrate (a radioactive compound). The test cell and deuterated mixture-cum-uranyl nitrate (UN) contents were modeled using MCNP5 to represent the physical systems described in published documents (Taleyarkhan et al., 2006a; Forringer et al., 2006a,b). 2.45 MeV neutrons were sourced into the middle of the test cell fluid and the transport characteristics through the test liquid, glass walls, and experiment enclosure was assessed using the Monte-Carlo method. The actual experimental geometry also included a layer (~5 cm thick) of paraffin blocks on three sides, and for one side of the enclosure for the experimental configurations of Taleyarkhan et al. (2006a) and of Forringer et al. (2006a,b), respectively. The paraffin blocks served as biological shielding material for experimenters. Fig. 4 displays representative results for the down-scattered neutron energy spectrum in terms of fraction of the total at the NE-213 LS detector face with and without the presence of the 3 cm thick ice-pack material. It is readily seen that the original 2.45 MeV neutron experiences significant down scattering resulting in a range of neutron energies down to thermal energy levels. The extent of down scattering is enhanced significantly with the addition of 3 cm of water (ice-pack) shielding. The displayed results have included all neutrons from 0 MeV to 0.1 MeV in a single energy bin, which accounts for the significantly larger counts for the first energy bin.

The resulting neutron energy spectrum was then used in conjunction with the SCINFUL code for modeling the response of

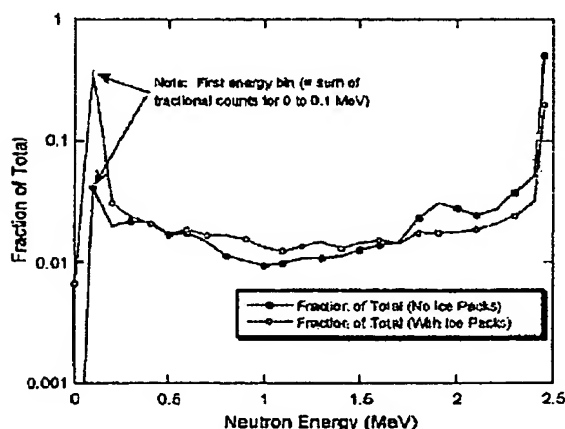


Fig. 4. MCNP5 computed neutron energy distribution for 2.45 MeV neutron after transport through 4 cm of test cell contents and then through 3 cm of ice-pack (modeled as water).

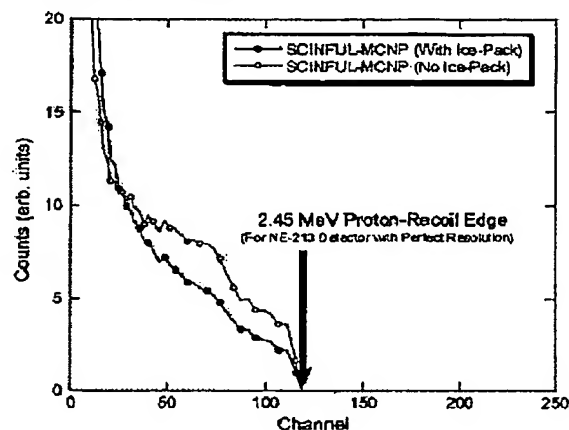


Fig. 5. Monte-Carlo simulation (SCINFUL-MCNP5) prediction of counts vs. light-output (pulse-height) for bubble fusion neutron spectra of Fig. 2 with and without ice-pack shielding.

NE-213 LS detectors to obtain the emanating light pulse-height response spectrum. In so doing, the MCNP5 predicted values for emitted neutron emission spectra of the type shown in Fig. 4 were utilized as inputs for the SCINFUL code to then derive the neutron spectral shapes (Fig. 5) with and without ice-pack shielding. Clearly the spectrum with ice-pack thermal shielding is noticeably different from the spectrum without ice-pack shielding and underscores the importance of accurately including intervening shielding materials. With the ice-pack materials included one notices a largely hyperbolic-like profile (reminiscent of the spectrum from a Cf-252 isotopic neutron source); without ice-pack shielding, the spectrum shape exhibits an anticipated hump starting from the PRE channel region.

Whereas, the spectrum with ice-packs appears qualitatively similar to that measured by Taleyarkhan et al. (as published in Fig. 4 of Taleyarkhan et al., 2006a,b), the calculated light output pulse-height spectrum without ice-pack shielding approximates the general characteristics of the spectrum measured by Forringer et al. (2006a,b), and by Taleyarkhan et al. (2004) and also to the spectrum calculated at UCLA (Naranjo, 2006) where the ice-pack thermal shield material was not included in the computational model. A more comprehensive comparison of data and predictions is provided below.

Next, the MCNP5–NE-213 model was used in which the MCNP5 results (Fig. 4) were binned and combined with the NE-213 LS detector response curves to arrive at the net response spectra of an LS detector for D–D fusion events within the test cell. As done for the MCNP5–SCINFUL model, results were obtained for the two cases with and without ice-pack shielding.

Results from the two approaches can now be compared against the Taleyarkhan et al. (2006a,b) measured neutron spectrum and the various results are shown in Fig. 6 for the experimental case (i.e., with ice-pack shielding). The corresponding results without ice-pack shielding are compared with the experimental measurements of Forringer et al. (2006a,b) as shown in Fig. 7. The reported UCLA predictions using GEANT (Naranjo, 2006) which were conducted without inclusion of intervening ice-pack shielding are also included in Fig. 7. We can now make the following observations:

- (i) Ref. Fig. 6: When ice-pack shielding is taken into account, the MCNP5–SCINFUL as well as the MCNP5–NE-213 predictions for

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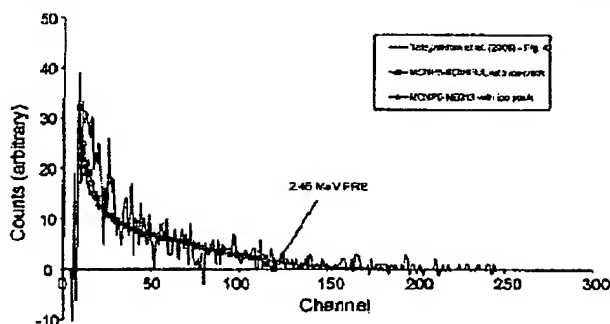


Fig. 6. Predictions of MCNP5–SCINFUL and MCNP5–NE-213 (Lee/Lee) methods vs. measured neutron response spectrum of Taleyarkhan et al. (2006a,b); with ice-pack shielding.

- the measured neutron spectrum are consistent with and compare very well with the measured and reported bubble fusion neutron spectrum (Taleyarkhan et al., 2006a,b). For this comparison, the Taleyarkhan et al. measured results at Channel 50 were scaled to equal the predicted value of counts from the MCNP5 based predictions (at the same channel), after which the same scale factor was used for all other channels.
- (ii) Ref. Fig. 6: Both MCNP5–SCINFUL and MCNP5–NE-213 predictions are consistent with each other below the 2.45 MeV PRE. Above the 2.45 MeV PRE, the MCNP5–SCINFUL model predicts no counts as would be expected. However, the MCNP5–NE-213 model's detector data-weighted predictions extend ~50 neutron channels above the 2.45 MeV PRE. This is a further confirmation that real-life detectors, with imperfect resolution characteristics, should be expected to allow neutron counts to be collected above the PRE channel. It also provides an important and independent corroboration for, and a valid reason for the excess counts measured (above the PRE) in the neutron spectrum during bubble fusion experiments (Taleyarkhan et al., 2006a,b).
  - (iii) Ref. Fig. 7: The MCNP5–NE-213 approach which is based on actual measurements offers results which are consistent with the MCNP5–SCINFUL and the public-source GEANT code predictions of UCLA. All three approaches are reasonably close to each other and consistent in terms of overall shape and quantity of counts to be expected below the 2.45 MeV PRE.

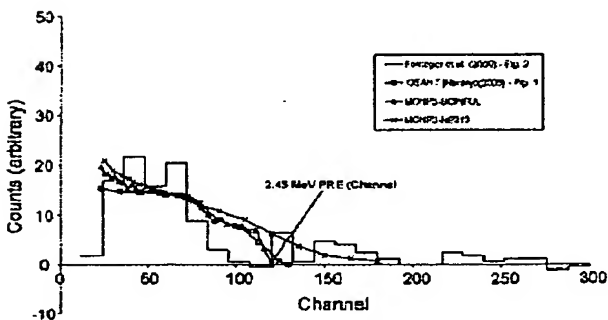


Fig. 7. Predictions of MCNP5–SCINFUL and MCNP5–NE-213 (Lee/Lee) methods vs. measured neutron response spectrum of Forringer et al. (2006a,b) (for no ice-pack shielding and scaled GEANT code predictions from Naranjo (2006).

- (iv) Ref. Fig. 7: The published bubble fusion neutron spectrum of Forringer et al. (2006a,b) which were obtained without intervening ice-pack shielding is consistent with and compares well with all three prediction schemes. The bubble fusion spectrum of Taleyarkhan et al. (2006a,b), and Forringer et al. (2006a,b) measurements both show counts above the 2.45 MeV PRE and this is also confirmed and predicted by using the MCNP5–NE-213 method.

#### 4.2. Comparison with external neutron nucleated bubble fusion experiments using deuterated acetone

We next turn attention to the earlier bubble fusion experiments of Xu et al. (2005) and Taleyarkhan et al. (2002, 2004). Both of these experimental studies were conducted using pure deuterated acetone as the test liquid. A key difference was that the Xu et al. experiments were seeded with randomly emitted neutrons of various energies from an isotopic neutron source, whereas, the Taleyarkhan et al. studies were conducted using 14 MeV monoenergetic neutrons from an accelerator. Another major difference involved the presence of ~3–4 cm of ice buildup at the freezer walls between the test cell and the LS detector for the Xu et al. (2005) studies, as shown schematically in Fig. 1c, whereas, there was no such intervening ice for the geometry (Fig. 1d) for the Taleyarkhan et al. (2002, 2004) studies.

##### 4.2.1. Comparison against the external neutron nucleated bubble fusion experiments of Xu et al. (2005)

MCNP5 modeling and analysis was conducted for the general geometry of the Xu et al. (2005) studies. Results of the downscattered 2.45 MeV neutrons for various amounts of ice-buildup are shown in Fig. 8a. Fig. 8b presents the variation of fractional down scattering of 2.45 MeV neutrons emitted from the test cell with ice thickness, and one notices the expected exponential-like trend. In Fig. 8a and b we note that due to the exponential downscattering behavior of neutron transport, errors in the actual ice buildup around the nominal 3 cm (~1 in.) value can be expected to remain small. As such, MCNP5–SCINFUL and MCNP5–NE-213 model simulations for the LS Detector response were conducted assuming the ice-buildup thickness of 3 cm.

Results of neutron pulse-height spectra are shown alongside the measured (published) data of Xu et al. (2005) in Fig. 9. It is clearly seen that, over the vast majority of the pulse-height spectrum the comparisons of the MCNP5–SCINFUL as well as MCNP5–NE-213 models are in very good agreement with the data.

##### 4.2.2. Comparison against external neutron nucleated bubble fusion experiments of Taleyarkhan et al. (2002, 2004)

A scoping experiment was also made to compare predictions of the modeling approach against the data obtained with 14.1 MeV externally nucleated bubble fusion experiments of Taleyarkhan et al. (2002, 2004). For the geometry of this experiment shown in Fig. 1d, there was no intervening ice-packing material between the test cell and the LS detector. Due to this aspect one would expect a sharp bump of counts around the 2.45 MeV PRE channel. A complexity arises due to the use of 14.1 MeV neutrons from the PNG for nucleating bubbles. The 14.1 MeV neutron results in a significantly high background due to which, excess counts due to 2.45 MeV neutrons emanating from the test cell, and which are above the 2.45 MeV PRE channel cannot be statistically discriminated from the large 14.1 MeV related background counts. Nevertheless, to decipher first-order effects, MCNP5 was used to model the test cell and detector alone surrounded by the ice-pack walls as shown in Fig. 1d. Due to this aspect, some discrepancies may be expected for the profile of the downscattered neutron energies reaching the LS

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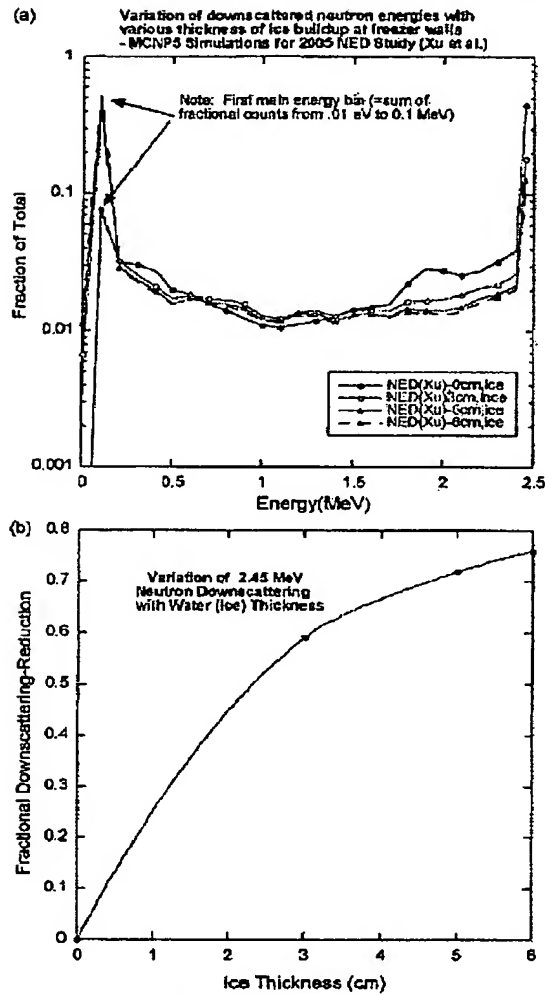


Fig. 8. (a) MCNP5 model predictions for variation of downscattered neutron energies for various thicknesses of ice buildup at freezer walls for externally nucleated experiments of Xu et al. (2005) with deuterated acetone. (b) Variation of fractional downscattering of 2.45 MeV neutrons with ice-thickness for Xu et al. experimental geometry (2005).

detector at the lower channels. Nevertheless, we were mainly interested to note if the principal trends from the MCNP5-SCINFUL and MCNP5-NE-213 model predictions are in general agreement with the published data of Taleyarkhan et al. (2004). Fig. 10 shows the MCNP5 results of downscattered neutrons at the LS detector volume for the geometry of Fig. 1d. Fig. 11 shows the MCNP5-SCINFUL and MCNP5-NE-213 model predictions versus the measurements. The comparisons indeed confirm that the overall trend is well-predicted. The measured spectrum is consistent with that of a 2.45 MeV neutron emitted from a D–D fusion event from within the test cell. In stark contrast to the comparisons against data taken with intervening ice-pack shielding (Fig. 9), when ice-packing is absent, we note a sharp bump in counts around the 2.45 MeV PRE channel in both the MCNP5-SCINFUL model predictions as well as for the measured spectrum of Taleyarkhan et al. (2004).

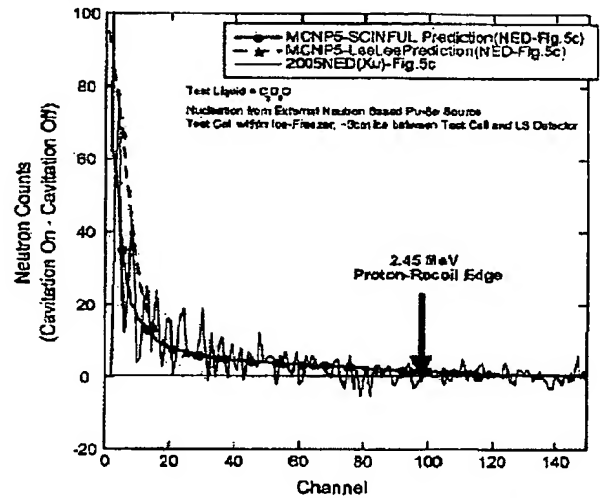


Fig. 9. Predictions of MCNP5-SCINFUL and MCNP5-NE-213 (Lee/Lee) models vs. measured neutron response spectrum (cavitation on-cavitation off) of Xu et al. (2005; Fig. 5c) with ice-pack shielding for external neutron nucleated fusion experiments with deuterated acetone.

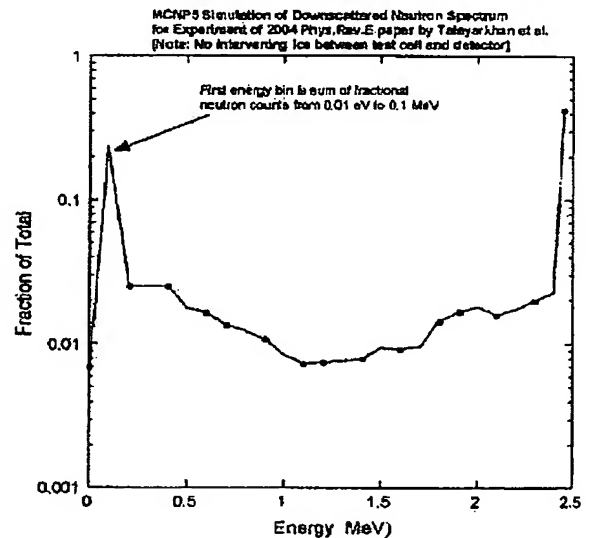


Fig. 10. MCNP5 predictions of down-scattered 2.45 MeV neutrons for Taleyarkhan et al. (2004) with 14 MeV PNG externally nucleated bubble fusion experiments.

## 5. Experiments and analyses to address the source of measured counts above the 2.45 MeV proton edge (PRE) for bubble fusion

In this section we provide observations and additional experimental data in relation to addressing the excess ("excess" means the additional counts above those from control experiments) counts that are seen above the 2.45 MeV PRE during our bubble fusion experiments using an NE-213 type LS detector. Overall, we have noted that up to ~95% of total excess neutron-gated counts are

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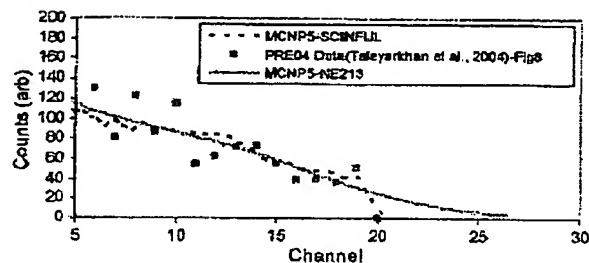


Fig. 11. MCNP5-SCINFUL and MCNP5-NE-213 model predictions vs. excerpted experimental data of Taleyarkhan et al. (2004; i.e., difference of counts from cavitation on minus cavitation off from Fig. 8c) with 14 MeV PNG externally nucleated bubble fusion experiments. Note: Counts above the 2.45 MeV PRE channel #21 are difficult to distinguish due to the large 14 MeV neutron background counts of about ~70–80 counts per channel.

obtained below the 2.45 MeV PRE. We have already covered one reason as being due to LS detector resolution, but other factors may also play a role. The source of additional counts above the 2.45 MeV PRE for the LS detector based results are believed to be due to the following phenomena.

#### 5.1. Finite detector resolution

Due to finite detector resolution, the 2.45 MeV PRE turns away from being a sharp rise at the maximum proton recoil energy of 2.45 MeV to a smeared shoulder (Knolls, 1999; Lee and Lee, 1998; Dickens, 1988) as already shown in the previous plots, Figs. 2–7. We estimate the spread to be in the range of up to ~50% light channels above the designated PRE. For our published bubble fusion data during self-nucleated acoustic cavitation, much of the excess counts above the 2.45 MeV PRE will occur within ~50 channels of the PRE channel number. However, beyond the first ~50 channels over the PRE, the finite resolution feature in itself cannot answer why excess counts appear in higher channels and as such, other potential contributors need to be evaluated.

#### 5.2. Imperfect PSD-related $\gamma$ leakage into the neutron window

In our 1/2006 PRL manuscript (Taleyarkhan et al., 2006a,b), we have pointed out that the PSD system settings were ~93% efficient in terms of gating out gamma photons. This implies that about 7% of gamma photons produced during bubble fusion will necessarily leak into the neutron window. For the geometry of the setup (Fig. 1 of Taleyarkhan et al., 2006a,b), the test cell was enclosed within ice-pack filled enclosure and in addition, there was significant paraffin biological shielding blocks in the vicinity. Neutrons produced from fusion would first downscatter, then interact with Cl atoms in the test liquid to produce ~1.0 MeV to ~1.5 MeV photons, but ultimately, with the abundance of hydrogen atoms around, neutron capture can also result in 2.2 MeV gamma photons. The light pulse-height from 2.2 MeV gamma photons encompasses the entire channel range of the multi-channel analyzer (MCA). Therefore, gamma photons could be readily counted above the 2.45 MeV PRE. As an estimate, using a NaI detector we had reported (Taleyarkhan et al., 2006a) an excess gamma photon count rate of ~0.55  $\gamma$ /s. A typical experiment lasting about 300 s would collect ~170 gamma photons, of which about 10% (~17) would be able to leak into the neutron window. From a typical excess neutron count population of about 1000 this amounts to about 1.5% of the total population.

#### 5.3. Neutron and gamma counts from fission with uranium in the test cell liquid

For experiments involving self-nucleation using alpha-recoils from uranium decay, the fission of uranium from D–D fusion neutrons may also theoretically lead to counts above the 2.45 MeV PRE channel. The well-established nuclear industry's MCNP5 nuclear particle transport code [developed and maintained at Los Alamos National Laboratory (LANL)] was utilized to assess the neutron spectrum emitted from the test cell. As noted in Fig. 4, a significant fraction of the 2.45 MeV neutrons will be down scattered to lower energies before escaping from surface. About 5–8% of the neutrons were calculated to be scattered down in the energy range of 0–1 eV. Considering the relatively small number density of  $^{235}\text{U}$  atoms and also  $^{238}\text{U}$  atoms (for which the fast fission threshold is below 2.45 MeV) a preliminary estimate reveals a rather small (<1%) fraction of the total excess neutron counts above the PRE that may result from fission. This phenomenon is not expected to be a significant contributor.

#### 5.4. D–T fusion reactions, or $^{13}\text{C}$ –n interactions

The deuterated test liquid includes a small quantity of tritium, T ( $^3\text{H}$ ) atoms and also a small fraction of the carbon, C atoms will be  $^{13}\text{C}$  for which possibilities exist to produce nuclear fusion signatures. However, these contributions are assessed as being negligibly small. Only the D–T reaction may produce 14 MeV neutrons and as such, only a rare, occasional count may appear in the higher channels. The D–T reactions may occur as a result of T atoms being produced during D–D fusion as also from the trace (orders of magnitude lower than that for D atoms) concentrations of T atoms in the procured deuterated liquid itself.

#### 5.5. Neutron pileup

A characteristic feature of acoustic inertial confinement (bubble) fusion is that the neutron emission is not continuous or random but implosion-based, and therefore, will be time-structured. Until recently, this aspect was not revealed as a possibility for excess neutron counts observed above the 2.45 MeV PRE. However, upon reconsideration and based on careful study of our recent theory paper published in the journal *Physics of Fluids* (Nigmatulin et al., 2005) new insights have been derived that appear to dictate that neutron pileup effects in LS detectors of the type used in the reported studies of Taleyarkhan et al. (2002, 2004, 2006a,b), Xu et al. (2005) and Forringer et al. (2006a,b) may indeed play a role in bubble fusion experiments. To further ascertain such an effect, we have conducted a series of experiments and analyses to quantify the relative contribution of neutron pileup (i.e., more than one neutron arriving at the detector within the detector's resolving time) during bubble fusion experimentation.

##### 5.5.1. Experiments and analyses for neutron pileup effect during bubble fusion experiments

The theory of super-compression (Nigmatulin et al., 2005), as applied to our bubble fusion experimentation has revealed that the bubble implosion process leading to D–D fusion for a single bubble in a rapidly imploding cluster occurs within the time span of ~0.1 ps and it will emit about 12 neutrons per bubble implosion. The estimated bubble cluster consisting of ~1000 bubbles is calculated to involve about 40 to 50 bubbles within the interior of the cluster where the amplification in implosion intensity produces thermonuclear fusion conditions. There is some uncertainty involved in terms of estimating the time scale over which the 40–50 bubbles implode but conservatively, we estimate that



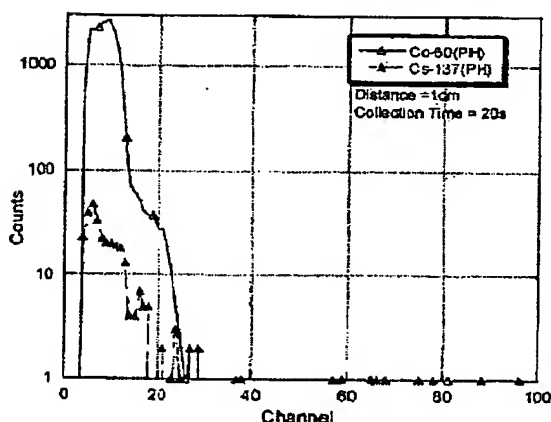


Fig. 12. Calibration spectra with  $^{60}\text{Co}$  and  $^{137}\text{Cs}$ .

they collectively will implode over 100 ps emitting a total of about 200–400 neutrons. This gives us an estimate of the instantaneous rate of neutron emission of up to  $\sim 4 \times 10^{12}$  n/s. This is a very high rate indeed and must be accounted for in terms of the possibility and consequence of more than one neutron arriving at the LS detector within the resolving (shaping) time of about  $\sim 100$  ns (which is considerably longer than the much shorter emission period, which lies in the ps range).

The assessment of possible neutron pileup effects on our LS detector was conducted both with a pulsed neutron source and also via theoretical scoping analyses.

**5.5.1.1. Experiments with a pulse neutron generator (PNG).** We employed a D–T accelerator driven PNG (Model NN-550 from Activation Technologies, Inc.) for assessing whether neutron pileup effects could materialize in our LS detector for neutron pulse rates in the vicinity of expected bubble fusion neutron pulse rates. The PNG system enabled stable operation down to 200 Hz during which neutron pulses are emitted over a time span of  $\sim 5$ – $6$   $\mu\text{s}$  (FWHM). The LS detector was placed with its face about 10 cm away from the PNG target. The LS detector response to  $^{60}\text{Co}$  and  $^{137}\text{Cs}$  sources was obtained. It was found (Fig. 12) that the  $^{60}\text{Co}$  1.2 MeV and 1.3 MeV gamma Compton edge is at channel  $\sim 15$ . From published light curves (Harvey and Hill, 1979) it would then imply that the 14.1 MeV PRE would appear around channel 105. With this calibration, the PSD spectrum was obtained and shown in Fig. 13. As previously noted, unlike that for an isotope-based neutron source, the D–T fusion based neutron source results in a much larger fraction of neutrons compared to gamma photons. D–T fusion does not produce gamma photons. Gamma photons are an indirect consequence of fusion neutron interactions with elements of surrounding structures. Based on calibrations with a 1 Ci Pu–Be source it was estimated that the PNG operating with a target voltage of  $\sim 50$  kV and 0.2 kHz would emit  $\sim 5 \times 10^5$  n/s, close to the maximum emission level allowed in our laboratory. Since these neutrons are emitted in pulses ( $\sim 10$   $\mu\text{s}$  wide at the base and  $\sim 5$   $\mu\text{s}$  FWHM) the instantaneous emission rate is much larger at  $\sim 5$ – $10 \times 10^8$  n/s ( $\sim 5 \times 10^5 / 5 \times 10^{-6} / 200$ ). This formed a baseline for estimating the instantaneous pulse neutron outputs at other target voltages.

Next, neutron-gated pulse-height spectra were obtained at various target voltages ranging from  $\sim 20$  kV to  $\sim 50$  kV. Results of pulse-height spectra are shown in Fig. 14 along with the total neutron counts versus drive voltage in Fig. 15. As expected, the 14.1 MeV PRE is seen to occur around channel #105. The rate of

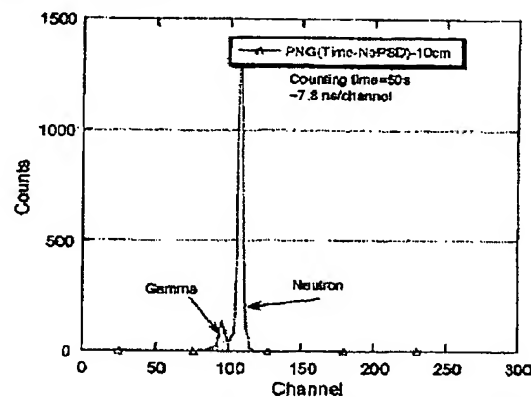


Fig. 13. Fusion (D–T) source PSD neutron–gamma spectrum with LS detector.

neutron counts increase is more rapid at smaller target voltages and decreases as the target voltage increases. This is in line with well-known ( $\sigma_v$ ) D–T reaction cross-sections (Gross, 1984). Fig. 14 clearly shows that, while insignificant excess counts are measured over the 14.1 MeV PRE at target voltages of less than  $\sim 40$  kV, the neutron pileup effect becomes noticeably larger for target voltage of  $\sim 40$  kV and above. The variation of the counts above the 14.1 MeV PRE with target voltage, expressed as a percentage is shown in Fig. 15. We see from Figs. 14 and 15 a rapid increase of neutron pileup induced counts above the PRE as the target voltage is increased.

The data shown in Fig. 14 were obtained with a source-to-detector distance of 10 cm compared with 30 cm in the published sonofusion experiments. This would imply a factor of  $\sim 10$  [ $\sim (30/10)^2$ ] difference based on solid angle effects, and to get about 3% of total counts above the PRE would require a rate of about  $10^{11}$  n/s. This level of output at a distance of about 30 cm is comparable to (even though smaller than) the estimated  $\sim 10^{12}$  n/s neutron emission rates for bubble fusion, thereby, forming a reasonable basis to expect that bubble fusion experiments with detection equipment of the type and configurations used will indeed lead to neutron-pileup related effects giving rise to excess counts above the PRE. The amount of excess may amount to  $\sim 5\%$  of the total neutron counts.

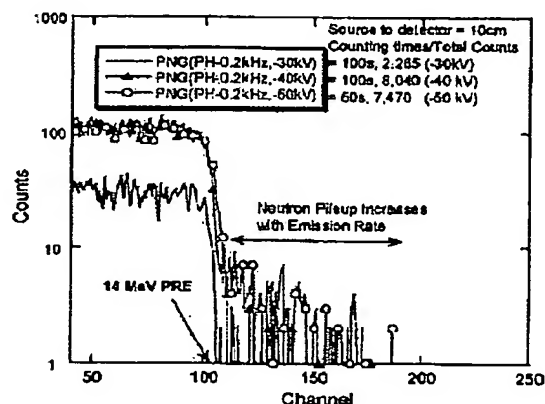


Fig. 14. Pulse-height spectra at various PNG target voltages (Note:  $\sim 50$  kV data were taken over 50 s not 100 s).



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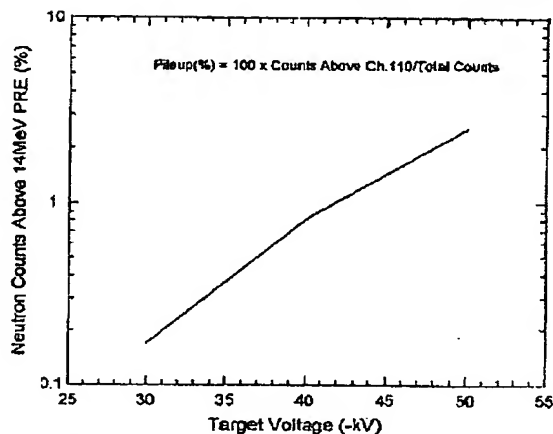


Fig. 15. Neutron pulse-pileup (%) vs. PNG target voltage.

**5.5.1.2. Analytic estimation of magnitude of neutron pileup.** If  $N$  neutrons are emitted during bubble cluster implosion such that they come within the resolving time of the detector, then the probability of a single neutron striking the detector is  $N \times f$ , where  $f$  is the fraction of the solid angle that the detector subtends.

The probability that two neutrons strike the same detector is  $N(N-1)f^2$ . If the detector efficiency is  $\epsilon$ , then the net probability requires that we multiply by  $\epsilon^2$ . The LS detector projects an area of about 25 cm<sup>2</sup> so that the solid angle " $f$ " at 30 cm from the test cell becomes 0.0022. Since we have estimated that up to 500 neutrons are emitted per bubble cluster implosion,  $N = 500$ . Based on known scattering cross-sections for C and H atoms, and the composition of NE-213 liquid, for a 5 cm  $\times$  5 cm LS detector, the mean free path for a 2.45 MeV neutron is calculated to be  $\sim 5.3$  cm. We can then assume that  $\sim 60\%$  of all neutrons would receive at least one collision within the LS liquid, which then would offer a theoretical intrinsic efficiency of at least  $\sim 50\%$ . Assuming a typical 50% detector (intrinsic) efficiency gives the net probability of the detector receiving two neutrons simultaneously  $= 500 \times 499 \times (0.0022)^2 \times (0.5)^2 = 0.3$  or about 30%. This methodology has assumed that each neutron regardless of energy striking the detector will contribute to the "pileup" effect equally. In reality, only neutrons above  $\sim 1.3$  MeV would be able to have an effect. From MCNP5 assessments the fraction of neutrons above 1.3 MeV is estimated to be  $\sim 40\%$  and  $\sim 80\%$  with and without ice-pack thermal shielding, respectively. This reduction would bring down the above-estimated 30% down to  $\sim 20\%$  [ $\sim 30\% \times (0.8)^2$ , without ice-packs] to  $\sim 5\%$  [ $\sim 30\% \times (0.4)^2$ , with ice-packs], respectively. The approach of this section necessarily encompasses uncertainties, chiefly related to the value of " $N$ ", but on an overall basis, it appears in line with and on the order of magnitude of neutron pileup as also witnessed from the experimental observations.

Based on the above, it may be reasonably expected on theoretical grounds that neutron pileup could play an important role in terms of providing excess counts above the 2.5 MeV PRE and the amount to be expected may be in the experimentally observed range of up to  $\sim 5\%$ – $10\%$  of the total neutron counts.

## 6. Summary and conclusions

In summary, a comprehensive framework has been developed to model, simulate and understand the 2.45 MeV neutron signature for acoustic inertial confinement (bubble) thermonu-

clear fusion signature. Both, self-nucleated and external neutron nucleated acoustic (bubble fusion) cavitation experiments have been modeled and analyzed for neutron spectral characteristics at the detector locations for all separate successful published bubble fusion studies. Monte-Carlo neutron transport calculations of 2.45 MeV neutrons from imploding bubbles were conducted, using the well-known MCNP5 transport code, for the published original experimental studies of Taleyarkhan et al. (2004, 2006a,b), as also the successful confirmation studies of Xu et al. (2005), Forringer et al. (2006a,b) and Bugg (2006). NE-213 LS detector response was calculated using the SCINFUL code. These were cross-checked using a separate and independent approach involving weighting and convoluting MCNP5 predictions with published experimentally measured NE-213 detector neutron response curves for monoenergetic neutrons at various energies. This resulted in the formulation of two models: (a) MCNP5–SCINFUL; (b) MCNP5–NE-213 models, respectively.

The MCNP5-based model was first successfully calibrated and validated against experimental data with an NE-213 based LS detector for three distinct neutron sources: (a) <sup>252</sup>Cf; (b) Pu–Be; (c) 14.1 MeV neutrons from a PNG accelerator device. Excellent agreement was demonstrated versus actual experimental data for neutron spectra with PSD.

The impact of neutron pulse-pileup during bubble fusion was verified and estimated with a pulsed neutron generator based experiments and theoretical analyses, both of which provided confidence that an implosion-based bubble fusion process will likely lead to pulse-pileup in the LS detector train. This aspect is consistent with theoretical predictions from our theory paper on super-compression of deuterium atom vapor filled imploding bubbles. Other major contributions and reasons for measurement of nuclear counts above the 2.45 MeV PRE channel were shown to be due to imperfect LS detector resolution around the PRE, gamma photon leakage due to imperfect PSD. The impact of uranium fission and other effects such as D–T or <sup>13</sup>C–n reactions were estimated to be of low order in importance.

The MCNP5–SCINFUL and MCNP5–NE-213 models were employed to model and predict the neutron spectra from LS detectors for all of the published data involving both self-nucleation experiments (Taleyarkhan et al., 2006a; Forringer et al., 2006a,b) as well as earlier experiments conducted with external neutron based nucleation experiments (Taleyarkhan et al., 2002, 2004; Xu et al., 2005). A key determinant for the neutron spectral shape was shown to be related to the presence or absence of intervening ice-pack thermal shielding between the test cell and the LS detector. The self-nucleation experiments of Taleyarkhan et al. (2006a,b) and external neutron nucleated experiments of Xu et al. (2005) included the presence of  $\sim 3$  cm of intervening ice-pack shielding between the LS detector and the test cell. However, the self-nucleated experiments of Forringer et al. (2006a,b) and the external neutron nucleated experiments of Taleyarkhan et al. (2002, 2004) did not include such intervening ice-pack shielding. All four experimental geometries were individually modeled using MCNP5 for deriving the transport characteristics of the 2.45 MeV fusion neutrons from within the test cell for each of the four experiments. The resulting neutron spectrum was next used to derive the LS detector spectral response using the MCNP5–SCINFUL and MCNP5–NE-213 models, respectively.

The results of modeling-cum-experimentation were found to be consistent with published experimentally observed neutron spectra for 2.45 MeV neutron emissions during acoustic cavitation (bubble) fusion experimental conditions with and without ice-pack (thermal) shielding. Calculated neutron spectra with inclusion of ice-pack shielding are consistent with the published spectra from the experiments of Taleyarkhan et al. (2006a,b) and Xu et al. (2005).

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where ice-pack shielding was present, whereas without ice-pack shielding the calculated neutron spectrum is consistent with the experimentally observed neutron spectrum of Taleyarkhan et al. (2002, 2004) and Forringer et al. (2006a,b). The reported GEANT code computer simulations of Naranjo (2006) were conducted with neglect of the intervening ice-pack shielding for the Taleyarkhan et al. (2006a,b) experiments. Since the Forringer et al. (2006a,b) study was conducted without intervening ice-pack shielding the published GEANT code simulation results were also compared against the Forringer et al. (2006a,b) reported spectrum. This comparison provided good overall agreement over the energy range of the reported data of Forringer et al. (2006a,b) and also with predictions from the MCNP5–SCINFUL and MCNP5–NE-213 model simulations.

The results of this manuscript confirm that the confusion and controversies caused from past reports (Reich, 2006; Naranjo, 2006) resulted from the neglect of important details and features of acoustic inertial confinement (bubble) nuclear fusion experiments and associated phenomenology.

Results from this paper demonstrate that ice-pack shielding between the detector and the fusion neutron source, gamma photon leakage and neutron pulse-pileup due to picosecond duration neutron pulse emission effects may play important role in affecting the spectra of 2.45 MeV D–D fusion neutrons from acoustic thermonuclear fusion experiments

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